

APPENDIX “A” STORM DRAINAGE EXHIBITS

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NOTES FOR STORM SEWER CONSTRUCTION

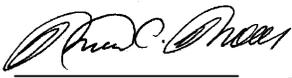
1. All construction and materials shall conform where applicable to the current Virginia Department of Transportation Road and Bridge Specifications.
2. All concrete shall be Class A3 if cast in place, Class A4 if precast.
3. Manholes and drop inlets shall be constructed from invert to top as follows:
 - A. Manholes to eight feet deep.
 - (1) Block construction - minimum eight inch walls.
 - (2) Poured in place concrete - minimum eight inch walls and nonreinforced.
 - (3) Precast - minimum eight inch walls in conjunction with precast throat and precast base slab.
 - (4) Precast.
 - B. Manholes over eight feet deep.
 - (1) Precast.
 - (2) Poured in place reinforced concrete.
 - (3) Special design, i.e., bends, precast tees, precast boxes, wyes.
4. Drop inlets and curb inlets shall have steps. The maximum dimension from finish grade to the first step in the inlet shall not exceed three feet.
5. Unless stated on the approved plans, symmetrical channels shall be installed in the invert of all structures according to VDOT standards IS-1 to prevent standing or ponding of water.
6. If block construction is used, the inside and outside walls, as they are laid, shall be plastered with mortar a minimum of 1/2" thick.
7. All precast drop inlets, curb inlets and manholes shall conform to ASTM C-478.
8. VDOT inlets where pipe size is larger than 48 inches I.D. require a special design. In case of special design inlets that deviate from the standard, the precast manufacturer or design engineer must submit five copies of detail drawings to the City of Manassas Public Works Department for proper approval.
9. The opening in precast storm sewer structures for all size pipe shall be a minimum of four inches and a maximum of six inches larger than the outside diameter of the pipe.
10. The "H" dimension shown on the standards and specified on the plans will be measured from the invert of the outfall pipe to the top of the structure.
11. Two (2) inch weep holes shall be provided in endwalls where directed by the City Site Inspector.
12. The contractor must notify the design engineer as to which will be precast so that the proper stakeout procedures can be followed.

GENERAL NOTES

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**CITY OF MANASSAS, VIRGINIA
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**COEFFICIENTS OF RUNOFF TO BE
USED WITH THE RATIONAL FORMULA**

<u>ZONE</u>		<u>"C" FACTOR</u>	<u>Tc (MIN)</u>
R-1, R-2, R-2-S	Residential (Average lot size)		
	a. 10,000 sq. ft. to 20,000 sq. ft.	0.35 - 0.45	10 - 15
	b. 20,000 sq. ft. to 5 Ac	0.30 - 0.40	10 - 15
A-1	Parks and Agriculture (over 5 acres)	0.25 - 0.35	to be computed
I-1	Cemeteries	0.25 - 0.35	to be computed
R-3	Townhouses	0.65 - 0.75	5 - 10
- -	Schools	0.50 - 0.60	10 - 15
R-5	Apartments	0.65 - 0.75	5 - 10
I-1, I-2	Industrial	0.80 - 0.90	5
B-1, B-2, B-3	Business, Commercial or Office	0.80 - 0.90	5
B-4	Residential Planned Community		

- NOTES:**
1. When calculating flow to a structure if all run-off to the structure is from impervious areas (i.e. pavement & roofs) the C to be used is 0.90.
 2. The lowest range of run-off coefficients may be used for flat areas (areas where the majority of the grades and slopes are 2% and less).
 3. The average range of run-off coefficients should be used for Intermediate areas (areas where the majority of the grades and slopes are from 2% to 5%).
 4. The highest range of run-off coefficients shall be used for steep areas (areas where the majority of the grades are greater than 5%), for cluster areas, and for development in clay soil areas.

COEFFICIENTS OF RUNOFF

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LAND USE DESCRIPTION	HYDROLOGIC SOIL GROUP			
	A	B	C	D
Cultivated land ^{1/} : without conservation treatment	72	81	88	91
: with conservation treatment	62	71	78	81
Pasture or range land: poor condition	68	79	86	89
good condition	39	61	74	80
Meadow: good condition	30	58	71	78
Wood or Forest land: thin stand, poor cover, no mulch	45	66	77	83
good cover ^{2/}	25	55	70	77
Open Spaces, lawns, parks, golf courses, cemeteries, etc.				
good condition: grass cover on 75% or more of the area	39	61	74	80
fair condition: grass cover on 50% to 75% of the area	49	69	79	84
Commercial and business areas (85% impervious)	89	92	94	95
Industrial districts (72% impervious)	81	88	91	93
Residential: ^{3/}				
Average lot size				
Average % impervious ^{4/}				
1/8 acre or less	65	77	85	90
1/4 acre	38	61	75	83
1/3 acre	30	57	72	81
1/2 acre	25	54	70	80
1 acre	20	51	68	79
Paved parking lots, roofs, driveways, etc. ^{5/}	98	98	98	98
Streets and roads:				
paved with curbs and storm sewers ^{5/}	98	98	98	98
gravel	76	85	89	91
dirt	72	82	87	89

^{1/} For a more detailed description of agricultural land use curve numbers refer to National Engineering Handbook, Section 4, Hydrology, Chapter 9, Aug. 1972.

^{2/} Good cover is protected from grazing and litter and brush cover soil.

^{3/} Curve numbers are computed assuming the runoff from the house and driveway is directed towards the street with a minimum of roof water directed to lawns where additional infiltration could occur.

^{4/} The remaining pervious areas (lawn) are considered to be in good pasture condition for these curve numbers.

^{5/} In some warmer climates of the country a curve number of 95 may be used.

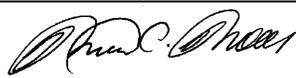
SOURCE: Urban Hydrology for Small Watersheds, SCS Technical Release No. 55, Table 2-2, January 1975.

RUNOFF CURVE NUMBERS FOR SELECTED AGRICULTURAL, SUBURBAN, AND URBAN LAND USE

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PERCENT IMPERVIOUSNESS FOR VARIOUS ZONING CLASSIFICATIONS*

Business and Commercial.....85%
Industrial.....75%
Schools and Churches.....60%

Residential

Apartments, Townhouses, Mobile Homes.....75%
1/4 Acre (R-10).....40%
1/3 Acre (R-20 Cluster).....35%
1/2 Acre (R-20).....30%
1 Acre (R-1-1).....25%
5 Acres and over.....15%

***Table may be used in lieu of computation of actual area of imperviousness.**

**PERCENT IMPERVIOUSNESS FOR
 VARIOUS ZONING CLASSIFICATIONS**

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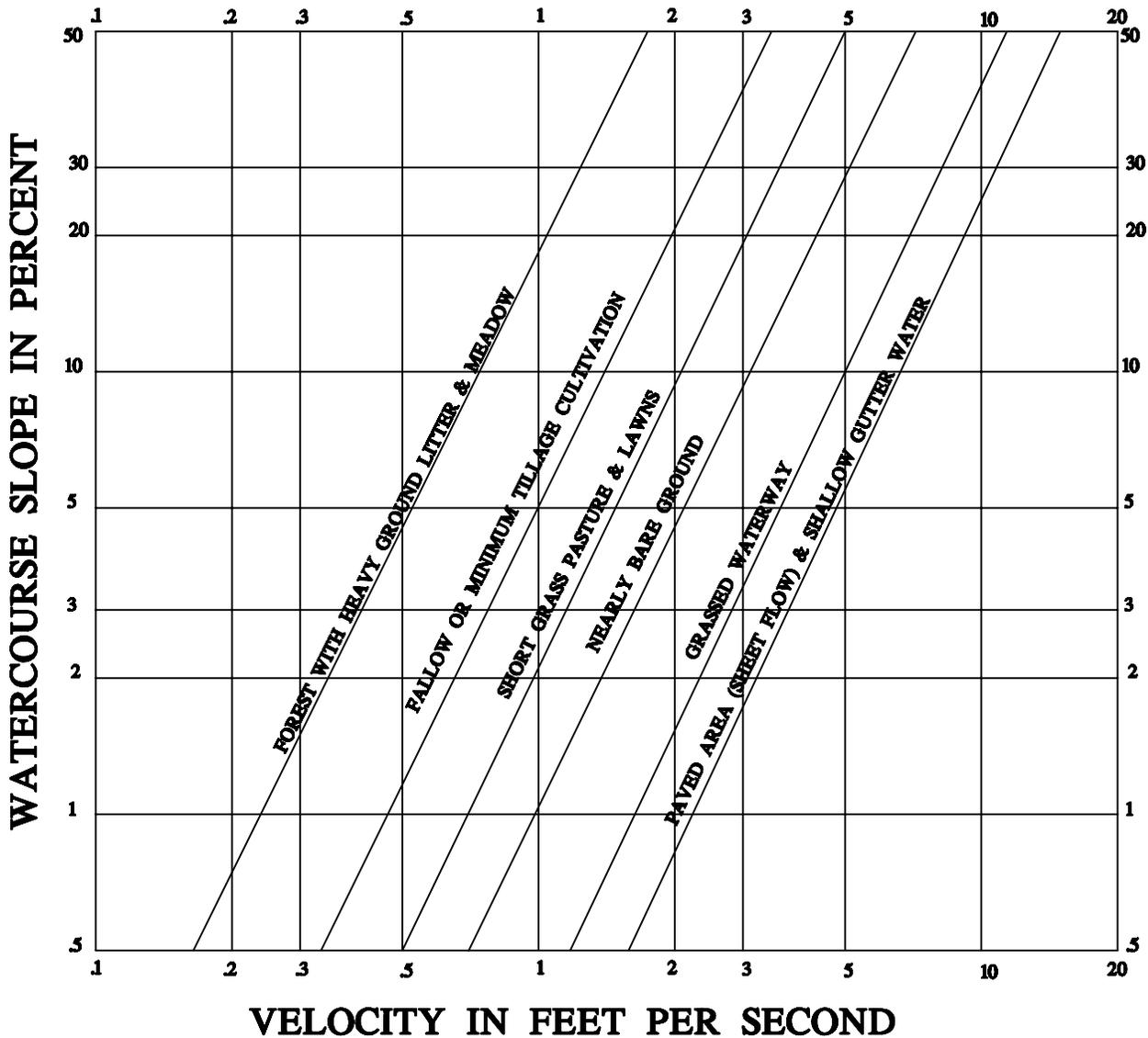


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SOURCE: URBAN HYDROLOGY FOR WATERSHEDS, TECHNICAL RELEASE NO. 55,
U.S. DEPARTMENT OF AGRICULTURE, JANUARY 1975.

AVERAGE VELOCITIES FOR ESTIMATING TIMES OF CONCENTRATION

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4

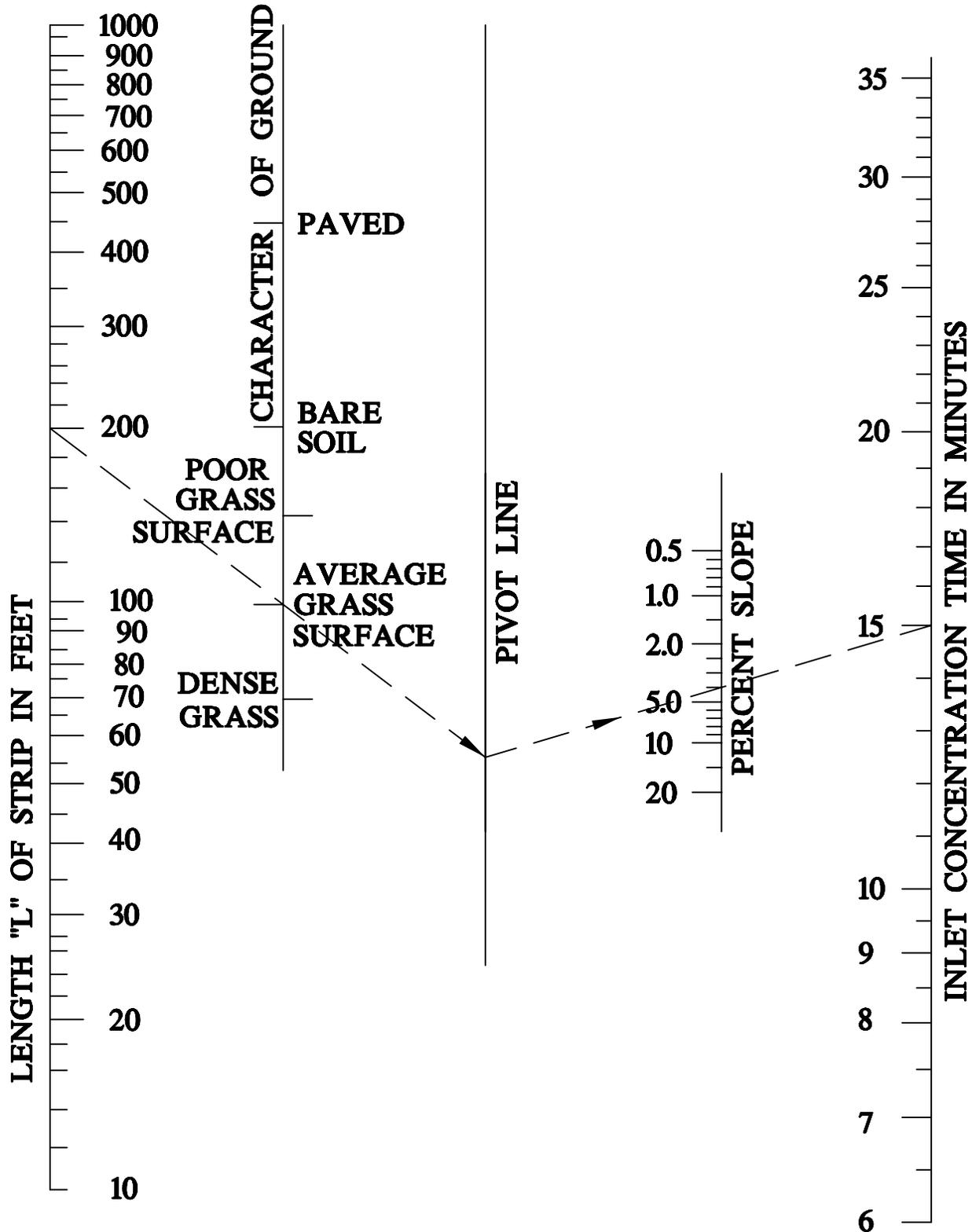
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**OVERLAND FLOW TIME
(USED WITH THE RATIONAL FORMULA)**

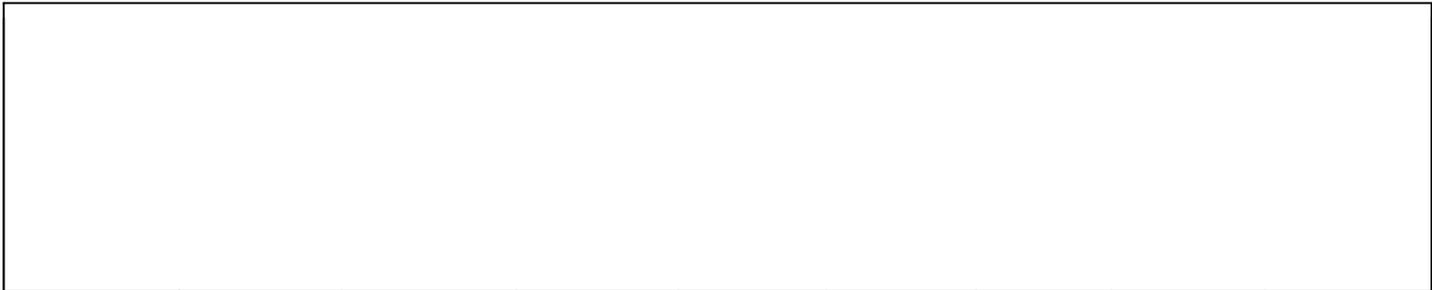
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Duration Frequency	5-Min.	15-Min.	1-Hour	2-Hour	3-Hour	6-Hour	12-Hour	24-Hour
2	0.46	0.90	1.50	2.0	2.1	2.6	3.1	3.4
5	0.54	1.11	1.91	2.5	2.7	3.3	3.8	4.5
10	0.59	1.26	2.20	3.0	3.2	3.9	4.7	5.3
25	0.68	1.47	2.61	3.5	3.7	4.3	5.2	6.0
50	0.74	1.63	2.93	4.0	4.3	5.1	6.0	7.0
100	0.81	1.80	3.25	4.4	4.8	5.8	6.4	7.8

SOURCES:

- NOAA Technical Memorandum, NWS HYDRO - 35
Five to 60-Minute Precipitation Frequency for the Eastern and Central U.S., 1977.
- U.S. Department of Commerce, Weather Bureau, Technical Paper No. 40 Rainfall Frequency Atlas of the United States, 1961.

**Rainfall Frequency-Duration-Depth relationships
(Rainfall Depth In Inches, Rainfall Frequency in Years)**

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Rainfall Intensity (INCHES PER HOUR)

Frequency	1-year	2-year	5-year	10-year	25-year	50-year	100-year
Duration							
5 minutes	4.26	5.23	6.06	6.77	7.69	8.39	9.10
10 minutes	3.40	4.19	4.89	5.45	6.15	6.76	7.28
15 minutes	2.83	3.51	4.13	4.62	5.22	5.77	6.22
30 minutes	1.94	2.41	2.88	3.26	3.73	4.20	4.57
1 hour	1.21	1.53	1.87	2.16	2.54	2.93	3.25
2 hours	0.711	0.868	1.10	1.28	1.54	1.75	1.97
3 hours	0.507	0.617	0.783	0.915	1.10	1.26	1.43
6 hours	0.312	0.379	0.479	0.560	0.682	0.785	0.897
12 hours	0.189	0.228	0.289	0.342	0.421	0.491	0.569
24 hours	0.109	0.132	0.170	0.203	0.254	0.299	0.351

PEAK RAINFALL INTENSITIES

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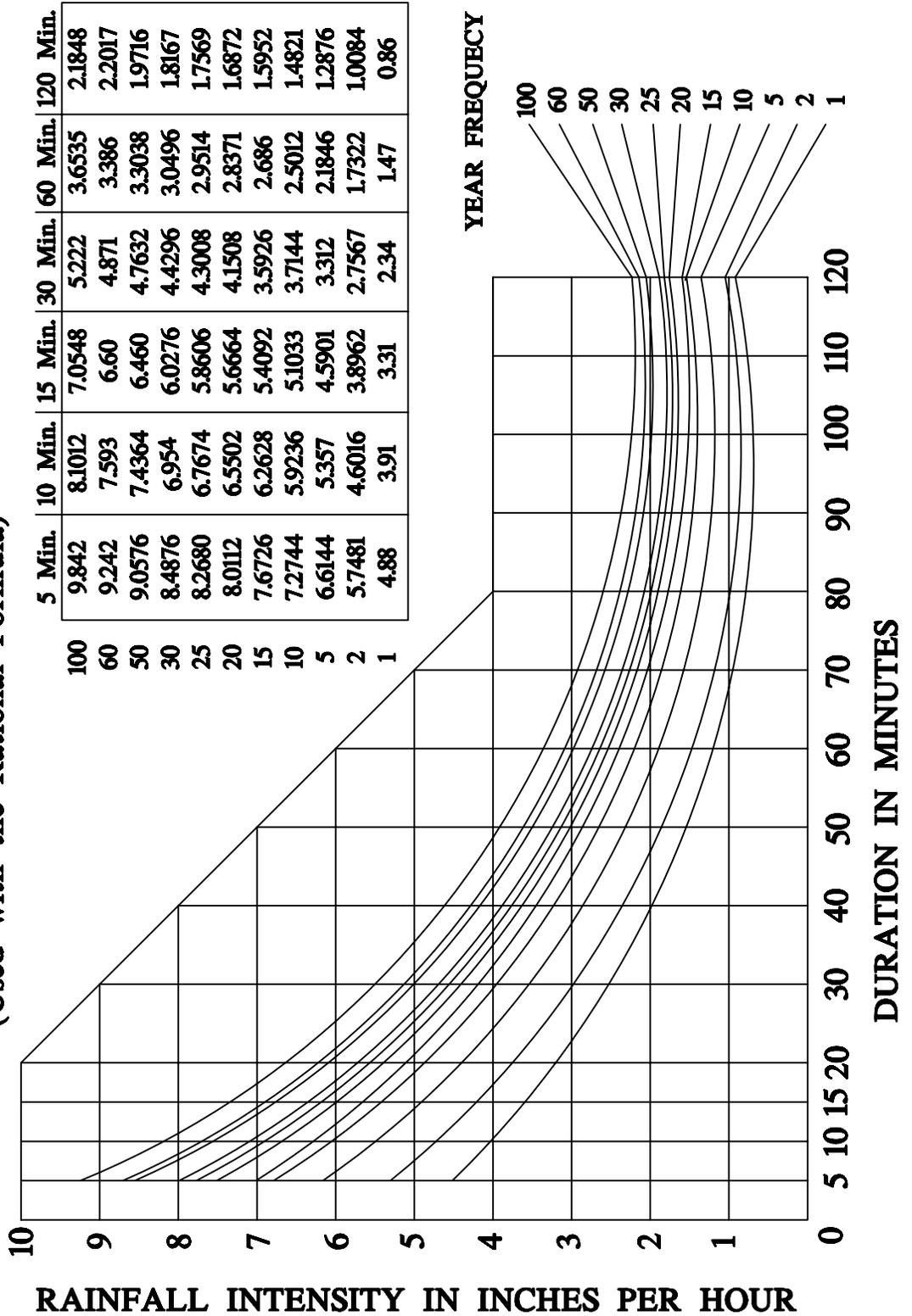
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**CURVES SHOWING
RAINFALL INTENSITY
vs.
DURATION FOR VARIOUS
FREQUENCES OF OCCURRENCE
(Used with the Rational Formula)**



**CURVES SHOWING RAINFALL INTENSITY
vs. DURATION OF OCCURRENCE**

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RADIUS OF CURVATURE FOR STRAIGHT DEFLECTED PIPE LENGTH OF 4 FEET												
Per Diameter in D Inches	Joint Opening in Inches											
	1/8	1/4	3/8	1/2	5/8	3/4	7/8	1	1-1/8	1-1/4	1-3/8	1-1/2
18	736	368	245	184	147	123	105	92	82	74	67	61
21	848	424	283	212	170	141	121	106	94	85	77	71
24	960	480	320	240	192	160	137	120	107	96	87	80
27	1072	536	357	268	214	179	153	134	119	107	97	89
30	1184	592	395	296	237	197	169	148	132	118	107	99
33	1296	648	432	324	259	216	185	162	144	130	118	108
36	1408	704	469	352	282	235	201	176	156	141	128	117
42	1632	816	544	408	326	272	233	204	181	163	148	136
48	1856	928	619	464	371	309	265	232	206	186	169	155
54	2080	1040	693	520	416	347	297	260	231	208	189	173
60	2304	1152	768	576	461	384	329	288	256	230	209	191
66	2528	1264	843	632	506	421	361	316	281	253	230	211
72	2752	1376	917	688	550	459	393	344	306	275	250	229
RADIUS OF CURVATURE FOR STRAIGHT DEFLECTED PIPE LENGTH OF 6 FEET												
18	1104	552	368	276	221	184	158	138	123	110	100	92
21	1272	636	424	318	254	212	182	159	141	127	116	106
24	1440	720	480	360	288	240	206	180	160	144	131	120
27	1608	804	536	402	322	268	230	201	179	161	146	134
30	1776	888	592	444	355	296	254	222	197	178	161	148
33	1944	972	648	486	389	324	278	243	216	194	177	162
36	2112	1056	704	528	422	352	302	264	235	211	192	176
42	2448	1224	816	612	490	408	350	306	272	245	223	204
48	2784	1392	928	696	557	464	398	348	309	278	253	232
54	3120	1560	1040	780	624	520	446	390	347	312	284	260
60	3456	1728	1152	864	691	576	494	432	384	346	314	288
66	3792	1896	1264	946	758	632	542	474	421	379	345	316
72	4128	2064	1376	1032	826	688	590	516	459	413	375	344
RADIUS OF CURVATURE FOR STRAIGHT DEFLECTED PIPE LENGTH OF 8 FEET												
18	1472	736	491	368	294	245	210	184	164	147	134	123
21	1696	848	565	424	339	283	242	212	188	170	154	141
24	1920	960	640	480	384	320	274	240	213	192	175	160
27	2144	1072	715	436	429	357	306	268	238	214	195	189
30	2368	1184	789	492	474	395	338	296	263	237	215	197
33	2592	1296	864	548	518	432	370	324	288	259	236	216
36	2816	1408	939	604	563	469	402	352	313	282	256	235
42	3264	1632	1088	716	653	544	466	408	363	326	297	272
48	3712	1856	1237	828	742	619	530	464	412	371	337	310
54	4160	2080	1387	940	832	693	594	520	462	416	378	347
60	4608	2304	1536	1052	922	768	658	576	512	461	419	384
66	5056	2528	1685	1164	1011	843	722	632	562	506	460	421
72	5504	2752	1835	1276	1101	917	786	688	612	550	500	459

RADIUS OF CURVATURE FOR CONCRETE PIPE

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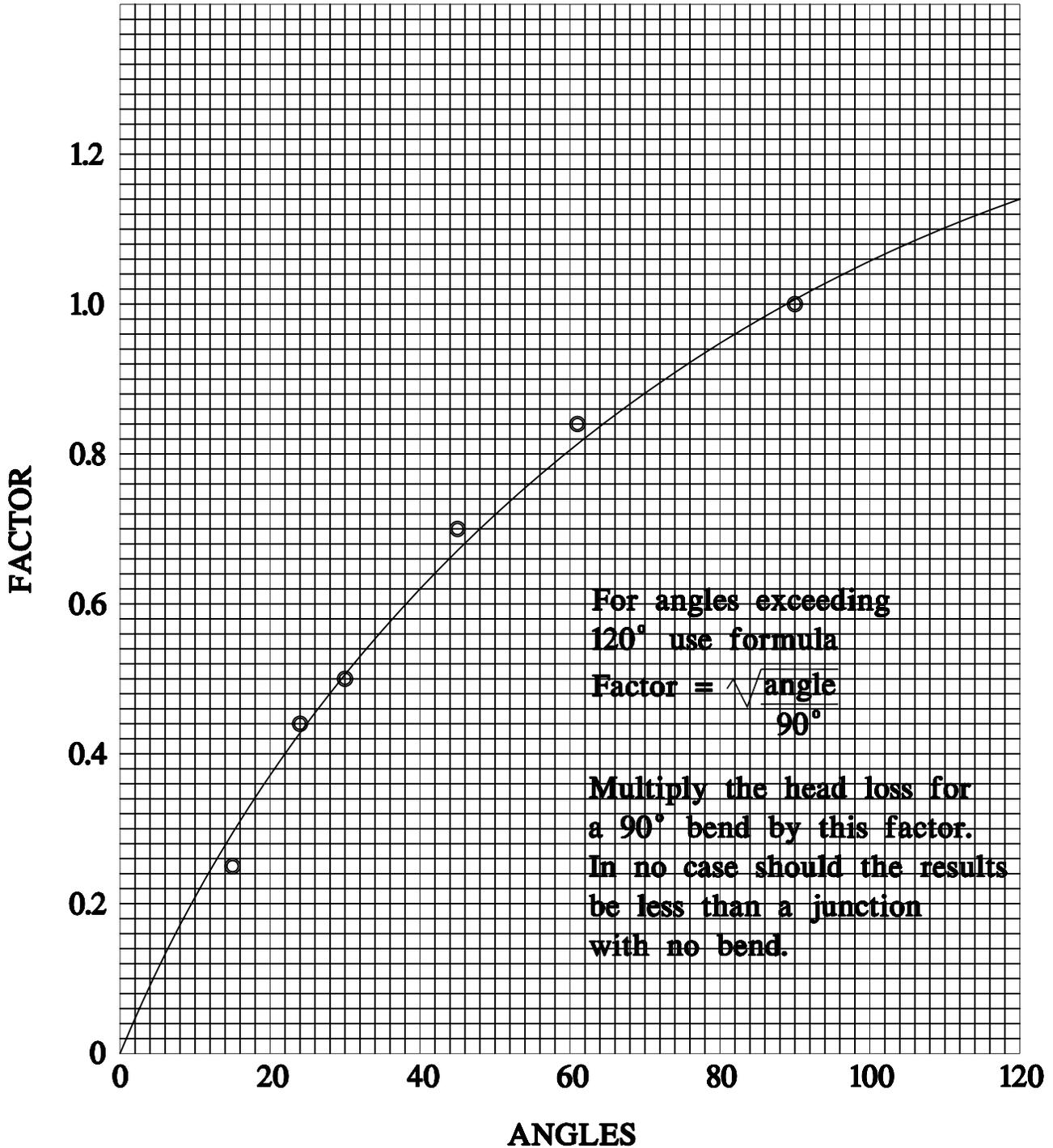
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**ANGLES OF BEND IN DEGREES
FACTORS OTHER THAN 90° BENDS**



ANGLE OF BEND IN DEGREES

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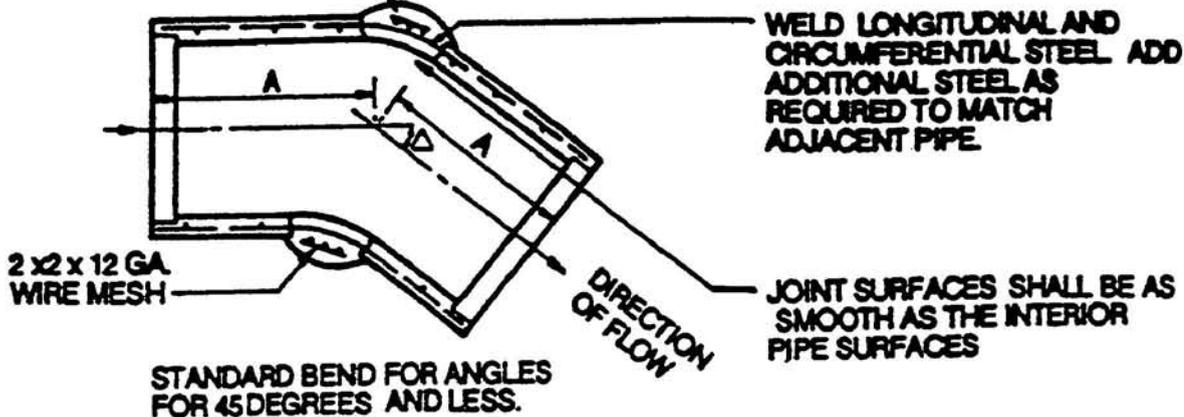
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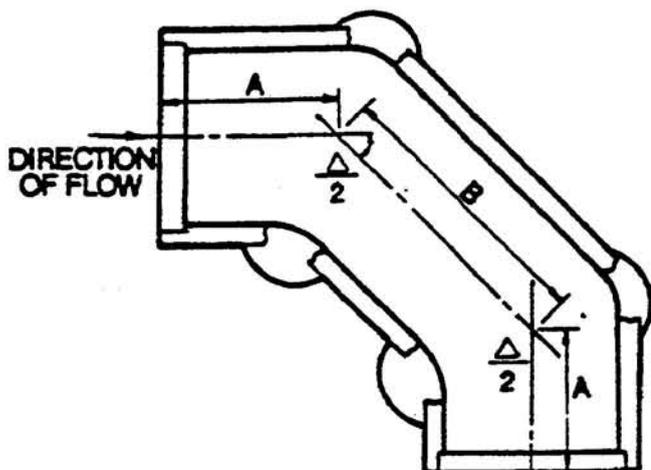
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STIFF MORTAR MIX
PLACED AROUND JOINT



STANDARD BEND FOR ANGLES
FOR 45 DEGREES AND LESS.



STANDARD BEND FOR ANGLES
BETWEEN 45 TO 90

PIPE SIZE	ANGLES 0°-45° A MIN.	ANGLES 45° TO 90° B MIN.
15"	1'-6"	-
18"	1'-6"	-
21"	2'-0"	-
24"	2'-0"	-
27"	2'-0"	-
30"	2'-0"	-
33"	2'-3"	2'-9"
36"	2'-3"	2'-9"
42"	2'-3"	3'-0"
48"	2'-6"	3'-3"
54"	2'-6"	3'-6"
60"	2'-9"	3'-6"

1. FOR PIPE SIZES 15" TO 30" IN DIA., BENDS NO GREATER THAN 30 DEGREES WILL BE ALLOWED UNLESS THERE ARE ACCESS OPENINGS WITHIN 50 FEET OF THE BEND.
2. FOR PIPE SIZES 33" TO 42" IN DIA., BENDS GREATER THAN 30° BUT LESS THAN 90° WILL BE ALLOWED PROVIDED THERE IS AN ACCESS OPENING WITHIN 50 FEET. BENDS UP TO 30 DEGREES HAVE NO RESTRICTION DISTANCE TO ACCESS OPENINGS.
3. THE USE OF THESE BENDS IS NOT ALLOWED WITHIN PUBLIC RIGHT - OF - WAYS.

NOT TO SCALE

REINFORCED CONCRETE PREFABRICATED BENDS

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PIPE CAPACITIES FLOWING FULL BY MANNING'S FORMULA

with n= 0.013 for concrete pipe

$$Q = a \times \frac{1.486}{0.013} \times \left(\frac{a}{p}\right)^{2/3} \times s^{1/2}$$

$$F = a \times \frac{1.486}{0.013} \times \frac{a^{2/3}}{p}$$

$$Q = F \times (s)^{1/2}$$

(s) values

PIPE DIAMETER, inches	F	Number	0	1	2	3	4	5	6	7	8	9
12"	35.64	.0001	.003162	.003317	.003464	.003606	.003742	.003873	.004000	.004123	.004243	.004359
15"	64.59	.0002	.004472	.004583	.004690	.004796	.004899	.005000	.005099	.005196	.005292	.005385
18"	105.04	.0003	.005477	.005598	.005657	.005745	.005831	.005916	.006000	.006083	.006164	.006245
21"	158.32	.0004	.006325	.006403	.006481	.006557	.006633	.006708	.006782	.006856	.006928	.007000
24"	226.20	.0005	.007071	.007141	.007211	.007280	.007348	.007416	.007483	.007550	.007616	.007681
27"	309.50	.0006	.007746	.007810	.007874	.007937	.008000	.008062	.008124	.008185	.008246	.008307
30"	410.20	.0007	.008367	.008426	.008485	.008544	.008602	.008660	.008718	.008775	.008832	.008888
33"	528.90	.0008	.008944	.009000	.009055	.009110	.009165	.009220	.009274	.009327	.009381	.009434
36"	666.60	.0009	.009487	.009539	.009592	.009644	.009695	.009747	.009798	.009849	.009899	.009950
42"	1006.10	.0010	.010000	.010050	.010100	.010149	.010198	.010247	.010296	.010344	.010392	.010440
48"	1436.00	.0011	.010000	.010049	.010095	.010140	.010183	.010225	.010265	.010304	.010342	.010378
54"	1965.00	.0012	.010144	.010149	.010183	.010217	.010249	.010281	.010312	.010342	.010371	.010398
60"	2604.00	.0013	.010173	.010176	.010179	.010181	.010184	.010187	.010189	.010192	.010194	.010195
66"	3357.00	.0014	.020000	.020025	.020049	.020074	.020098	.020121	.020145	.020168	.020191	.020214
72"	4234.00	.0015	.02236	.02236	.02236	.02236	.02236	.02236	.02236	.02236	.02236	.02236
78"	5242.00	.0016	.02449	.02470	.02490	.02510	.02530	.02550	.02569	.02588	.02606	.02627
84"	6387.00	.0017	.02646	.02665	.02683	.02702	.02720	.02739	.02757	.02775	.02793	.02811
90"	7679.00	.0018	.02828	.02846	.02864	.02881	.02898	.02915	.02933	.02950	.02966	.02983
96"	9119.00	.0019	.03000	.03017	.03033	.03050	.03066	.03082	.03098	.03114	.03130	.03146
102"	10720.00	.0020	.03162	.03178	.03194	.03209	.03225	.03240	.03256	.03271	.03286	.03302
108"	12490.00	.0021	.03162	.03317	.03464	.03606	.03742	.03873	.04000	.04123	.04243	.04359
114"	14420.00	.0022	.04472	.04583	.04690	.04796	.04899	.05000	.05099	.05196	.05292	.05385
120"	16540.00	.0023	.05477	.05568	.05657	.05745	.05831	.05916	.06000	.06083	.06164	.06245
		.0024	.06325	.06403	.06481	.06557	.06633	.06708	.06782	.06856	.06928	.07000
		.0025	.07071	.07141	.07211	.07280	.07348	.07416	.07483	.07550	.07616	.07681
		.0026	.07746	.07810	.07874	.07937	.08000	.08062	.08124	.08185	.08246	.08307
		.0027	.08367	.08426	.08485	.08544	.08602	.08660	.08718	.08775	.08832	.08888
		.0028	.08944	.09000	.09055	.09110	.09165	.09220	.09274	.09327	.09381	.09434
		.0029	.09487	.09539	.09592	.09644	.09695	.09747	.09798	.09849	.09899	.09950
		.0030	.10000	.10050	.10100	.10149	.10198	.10247	.10296	.10344	.10392	.10440
		.0031	.1000	.1049	.1095	.1140	.1183	.1225	.1265	.1304	.1342	.1378
		.0032	.1414	.1449	.1483	.1517	.1549	.1581	.1612	.1643	.1673	.1703
		.0033	.1732	.1761	.1789	.1817	.1844	.1871	.1897	.1924	.1949	.1975
		.0034	.2000	.2025	.2049	.2074	.2098	.2121	.2145	.2168	.2191	.2214
		.0035	.2236	.2236	.2236	.2236	.2236	.2236	.2236	.2236	.2236	.2236
		.0036	.2449	.2470	.2490	.2510	.2530	.2550	.2569	.2588	.2606	.2627
		.0037	.2646	.2665	.2683	.2702	.2720	.2739	.2757	.2775	.2793	.2811
		.0038	.2828	.2846	.2864	.2881	.2898	.2915	.2933	.2950	.2966	.2983
		.0039	.3000	.3017	.3033	.3050	.3066	.3082	.3098	.3114	.3130	.3146
		.0040	.3162	.3178	.3194	.3209	.3225	.3240	.3256	.3271	.3286	.3302

To obtain Q, multiply F by the square root of the slope, S, in ft. per ft.

To utilize this table for values of n* other than 0.013, first obtain Q based on 0.013, then multiply this Q by the ratio: other value of n divided into .013.

The full flowing capacity of the pipe should equal or exceed the 10 year storm water runoff.

In reviewing the adequacy of submitted designs, first check the capacity by graphic methods.

If this check indicates a border-line case where the pipe size may or may not be adequate

use this table to compute the capacity of the pipe.

Q in cubic feet per second n is friction factor

a is cross sectional area, square feet

p is wetted perimeter, feet, the inside circumference of the pipe

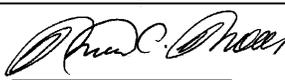
s is pipe slope in ft. per ft.

1.486 is a constant

*n = .024 plain CMP n = .021 paved CMP

**PIPE CAPACITIES FLOWING FULL
BY MANNING'S FORMULA**

REVISION & DATE

 3/4/97
DIRECTOR DATE

**CITY OF MANASSAS, VIRGINIA
DEPARTMENT OF PUBLIC WORKS**

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12

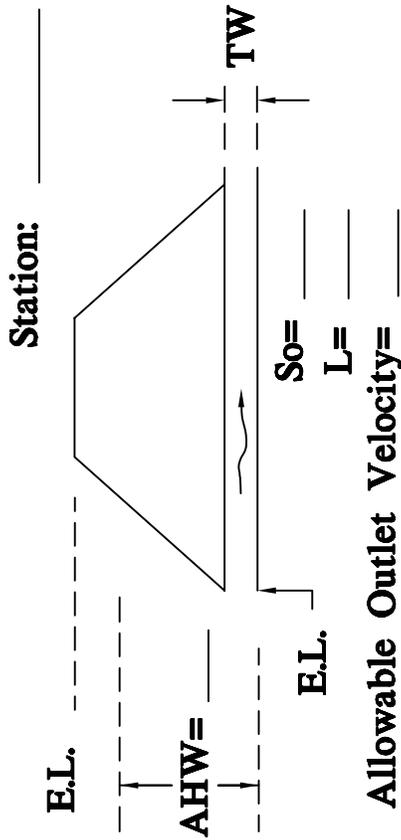
Project:

Designer:
Date:

Hydrologic and Channel Information

$Q_1 =$
 $Q_2 =$
 $TW_1 =$
 $TW_2 =$

SKETCH



Culvert Type	Q	Size	Headwater Computation				Controlling MH	Outlet Velocity	Cost	Comments									
			Inlet Cont.		Outlet Control														
			$\frac{HW}{D}$	HW	Kc	dc					$\frac{dc+O}{2}$	ho	H	LSo	HW				

Summary & Recommendations:

CULVERT DESIGN FORM

REVISION & DATE

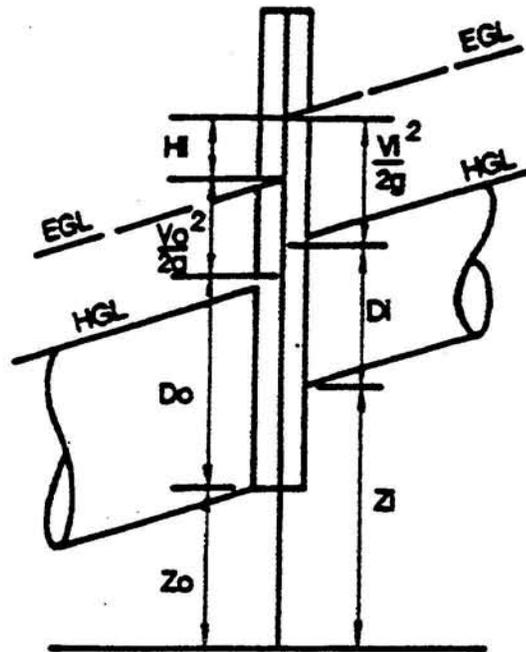
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[Signature] 3/4/97
DIRECTOR DATE

CITY OF MANASSAS, VIRGINIA
DEPARTMENT OF PUBLIC WORKS

13

- EGL = ENERGY GRADE LINE
- HGL = HYDRAULIC GRADE LINE
- h = ENERGY LOSS THROUGH A BEND
- H = ENERGY LOSS THROUGH EXPANSION
- ho = ENERGY LOSS THROUGH CONTRACTION
- Hl = TOTAL ENERGY LOSS THROUGH A JUNCTION



BEND ANGLE	C FACTOR
90	0.70
80	0.66
70	0.61
60	0.55
50	0.47
40	0.38
30	0.28
25	0.22
20	0.16
15	0.10

$$Hl = H + h_o + h$$

$$h = C \times \frac{V_i^2}{2g}$$

$$h_o = 0.25 \frac{V_o^2}{2g}$$

$$H = 0.35 \frac{V_i^2}{2g}$$

$$\text{NON - PRESSURE FLOW}$$

$$\text{DROP} = Z_i - Z_o = (D_o - D_i) + \left(\frac{V_o^2}{2g} - \frac{V_i^2}{2g} \right) + Hl$$

- Z_i, Z_o = INCOMING AND OUTGOING PIPE INVERT
- D_i, D_o = INCOMING AND OUTGOING DEPTH OF FLOW
- P_i, P_o = INCOMING AND OUTGOING PRESSURE HEADS
- $\frac{V_i^2}{2g}, \frac{V_o^2}{2g}$ = INCOMING AND OUTGOING VELOCITY HEADS

HYDRAULIC GRADE LINE IN CLOSED PIPE JUNCTION

REVISION & DATE

EXHIBIT NUMBER

M.C. Perry 4/19/96
DIRECTOR DATE

CITY OF MANASSAS, VIRGINIA
DEPARTMENT OF PUBLIC WORKS

16

H_p AND SLOPE RANGE AT RETARDANCE VALUES FOR VARIOUS DISCHARGES, VELOCITIES, AND CREST LENGTHS

	MAXIMUM		H _p				SLOPE	
	VELOCITY	DISCHARGE	L(ft)				MIN.	MAX.
	V	q	25	50	100	200		
	ft/s	ft ³ /s/ft	ft	ft	ft	ft	pct	
Retardance A	3	3	2.3	2.5	2.5	2.5	1	11
	4	4	2.3	2.5	2.8	3.1	1	12
	4	5	2.5	2.6	2.9	3.2	1	7
	5	6	2.6	2.7	3.0	3.3	1	9
	6	7	2.7	2.8	3.1	3.5	1	12
	7	10	3.0	3.2	3.4	3.8	1	9
	8	12.5	3.3	3.5	3.7	4.1	1	10
	Retardance B	2	1	1.2	1.4	1.5	1.8	1
2		1.25	1.3	1.4	1.6	1.9	1	7
3		1.5	1.3	1.5	1.7	1.9	1	12
3		2	1.4	1.5	1.7	1.9	1	8
4		3	1.6	1.7	1.9	2.2	1	9
5		4	1.8	1.9	2.1	2.4	1	8
6		5	1.9	2.1	2.3	2.5	1	10
7		6	2.1	2.1	2.4	2.7	1	11
Retardance D	2	0.5	0.6	0.7	0.8	0.9	1	6
	3	1	0.8	0.9	1.0	1.1	1	6
	3	1.25	0.8	0.9	1.0	1.2	1	4
	4	1.25	0.8	0.9	1.0	1.2	1	10
	4	2	1.0	1.1	1.3	1.4	1	4
	5	1.5	0.9	1.0	1.2	1.3	1	12
	5	2	1.0	1.2	1.3	1.4	1	9
	5	3	1.2	1.3	1.5	1.7	1	4
	6	2.5	1.1	1.2	1.4	1.5	1	11
	6	3	1.2	1.3	1.5	1.7	1	7
	7	3	1.2	1.3	1.5	1.7	1	12
	7	4	1.4	1.5	1.7	1.9	1	7
	8	4	1.4	1.5	1.7	1.9	1	12
8	5	1.6	1.7	1.9	2.0	1	8	
10	6	1.8	1.9	2.0	2.2	1	12	
Retardance E	2	0.5	0.5	0.5	0.6	0.7	1	2
	3	0.5	0.5	0.5	0.6	0.7	1	9
	3	1	0.7	0.7	0.8	0.9	1	3
	4	1	0.7	0.7	0.8	0.9	1	6
	4	1.25	0.7	0.8	0.9	1.0	1	5
	5	1	0.7	0.7	0.8	0.9	1	12
	5	2	0.9	1.0	1.1	1.2	1	4
	6	1.5	0.8	0.9	1.0	1.1	1	12
	6	2	0.9	1.0	1.1	1.2	1	7
	6	3	1.2	1.2	1.4	1.5	1	4
	7	2	0.9	1.0	1.1	1.2	1	12
	7	3	1.2	1.2	1.3	1.5	1	7

H_p & SLOPE AT RETARDANCE VALUES

REVISION & DATE

EXHIBIT NUMBER

17

M.C. Perry 4/19/96
DIRECTOR DATE

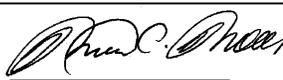
CITY OF MANASSAS, VIRGINIA
DEPARTMENT OF PUBLIC WORKS

INCREMENTAL UNIT HYDROGRAPH VALUES

REVISION & DATE

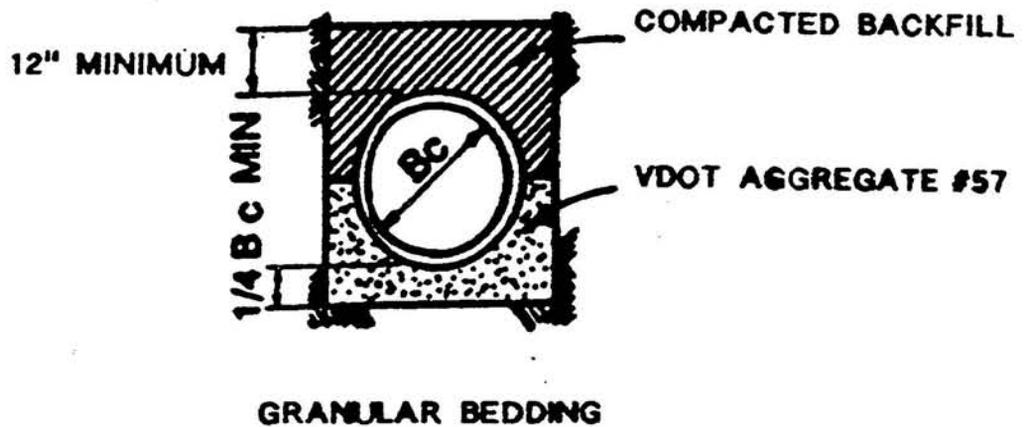
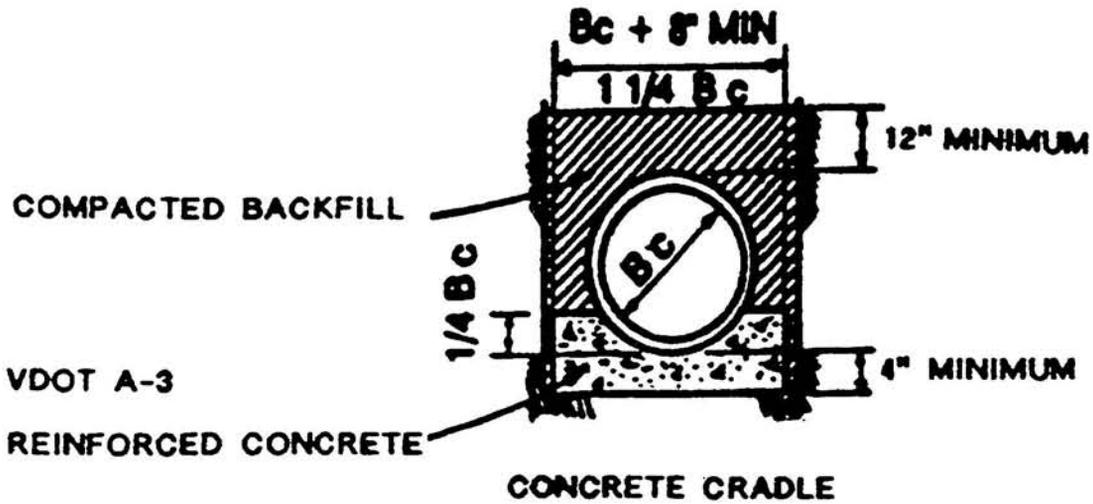
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 4/19/96
 _____ DATE
 DIRECTOR

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DEPARTMENT OF PUBLIC WORKS

Time Tc	5	10	15	20	25	30	35	40	45	50	55	60	65	70	75	80	85	90
10 - Year	7.27	4.68	3.46	2.77	2.29	1.94	1.68	1.47	1.31	1.18	1.08	0.99						
100 - Year	3.25	5.92	4.53	3.14	2.43	1.99	1.67	1.41	1.21	1.04	0.92	0.80						
10 - Year	2.20	4.24	5.10	4.36	3.08	2.34	1.89	1.56	1.29	1.07	0.89	0.73						
100 - Year	1.98	3.37	4.20	4.56	4.16	3.02	2.22	1.83	1.58	1.41	1.27	1.17						
10 - Year	1.28	2.40	3.25	3.83	4.03	3.89	3.35	2.68	2.05	1.58	1.29	1.12						
100 - Year	0.80	1.57	2.32	3.00	3.52	3.71	3.48	3.03	2.49	1.97	1.58	1.32	1.11	0.97				
10 - Year	9.84	6.37	4.73	3.74	3.13	2.65	2.33	2.07	1.88	1.69	1.55							
100 - Year	3.68	8.10	6.47	4.44	3.50	2.86	2.43	2.17	1.93	1.78	1.67	1.58						
10 - Year	2.81	5.99	7.05	5.69	3.89	3.17	2.73	2.40	2.16	1.98	1.83	1.68						
100 - Year	1.43	3.36	5.33	6.32	5.15	3.78	3.03	2.55	2.23	2.00	1.87	1.75						
10 - Year	0.98	2.26	3.79	5.05	5.75	5.17	3.99	2.90	2.28	1.96	1.77	1.65	1.53	1.43	1.39			
100 - Year	0.97	1.88	2.80	3.79	4.73	5.22	4.78	3.92	3.04	2.52	2.20	1.97	1.81	1.65	1.55	1.51	1.49	1.45



NOTE:

- A. IN ROCK TRENCH, EXCAVATE AT LEAST 6 IN. (15 CM) BELOW THE BELL OF THE PIPE EXCEPT WHERE CONCRETE CRADLE IS USED.

NOT TO SCALE

PIPE BEDDING FOR STORM SEWER LINES

REVISION & DATE

EXHIBIT NUMBER

19

DIRECTOR

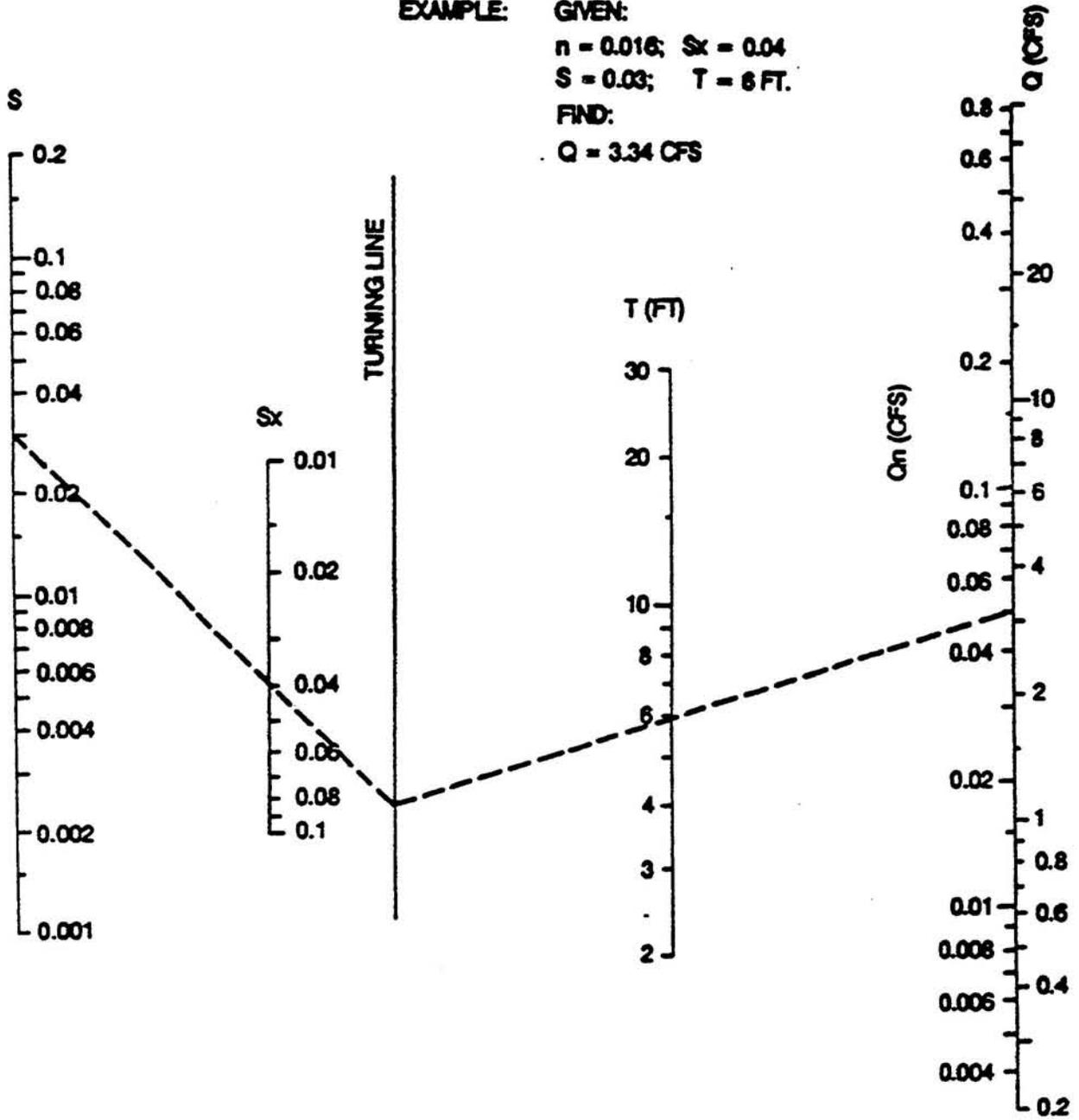
DATE

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D. C. May 4/19/96

$$Q = \frac{0.56 S_x^{1.67} S^{0.5} T^{2.67}}{n}$$

EXAMPLE: GIVEN:
 n = 0.016; S_x = 0.04
 S = 0.03; T = 6 FT.
 FIND:
 Q = 3.34 CFS



FLOW CHART TRIANGULAR GUTTER SECTIONS

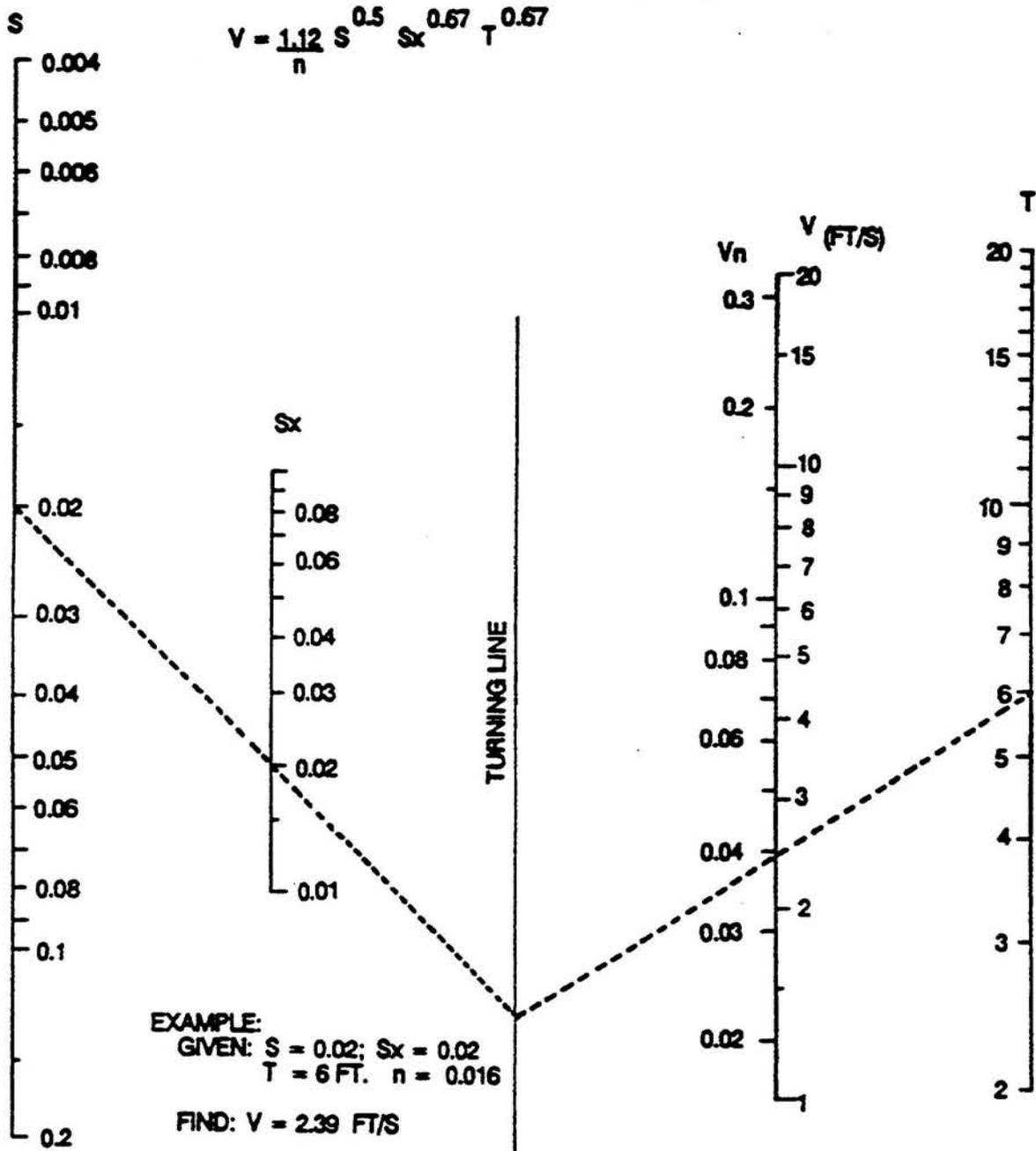
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D.C. [Signature] 4/19/96
 DIRECTOR DATE



VELOCITY CHART TRIANGULAR GUTTER SECTIONS

REVISION & DATE

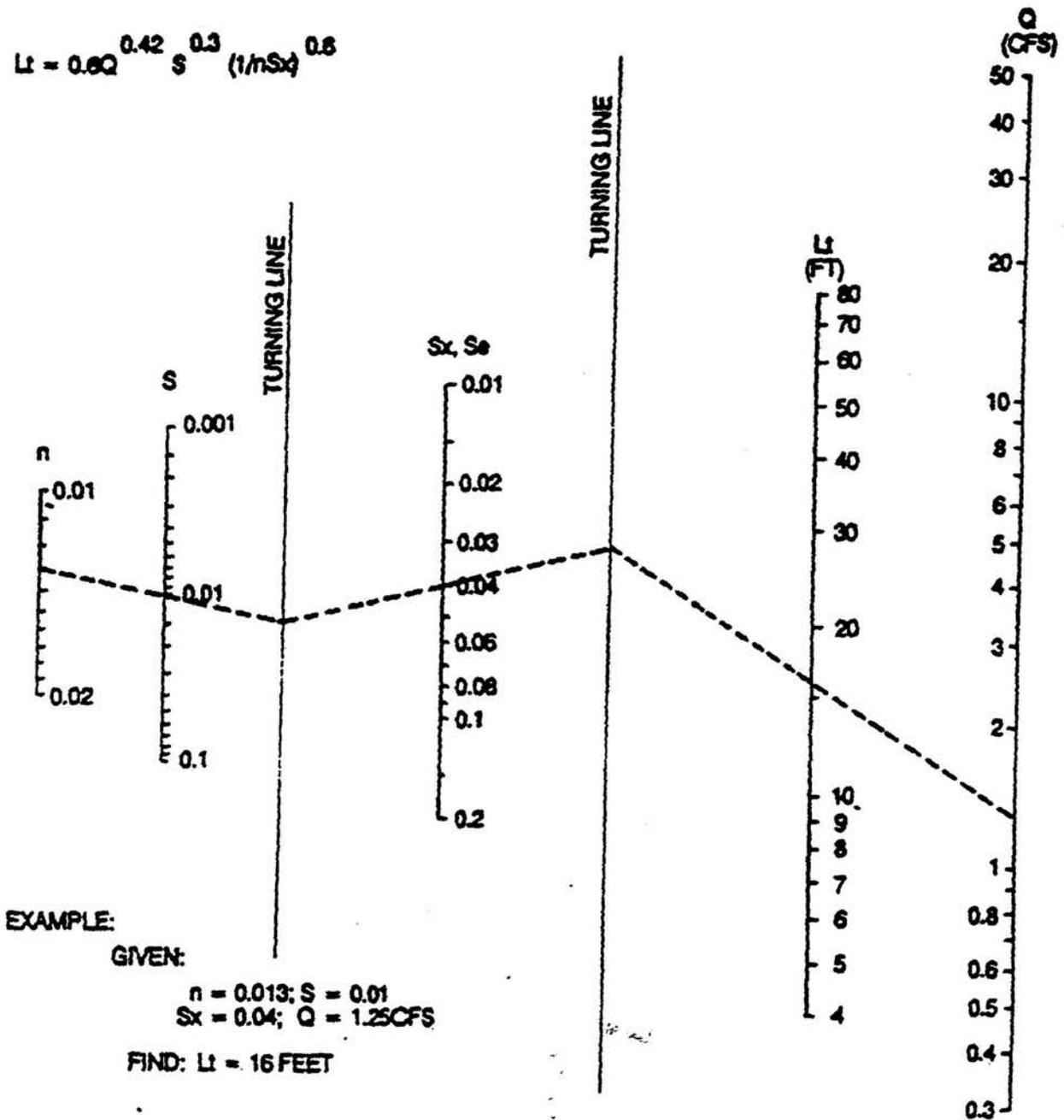
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P.C. Price 4/19/96
 DIRECTOR DATE

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$$L_i = 0.8Q^{0.42} S^{0.3} (1/nS^4)^{0.8}$$



CURB INLET DESIGN CHART ON GRADE CONDITION

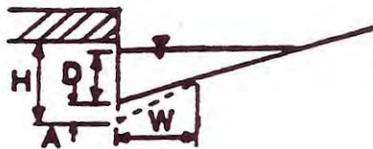
REVISION & DATE

EXHIBIT NUMBER

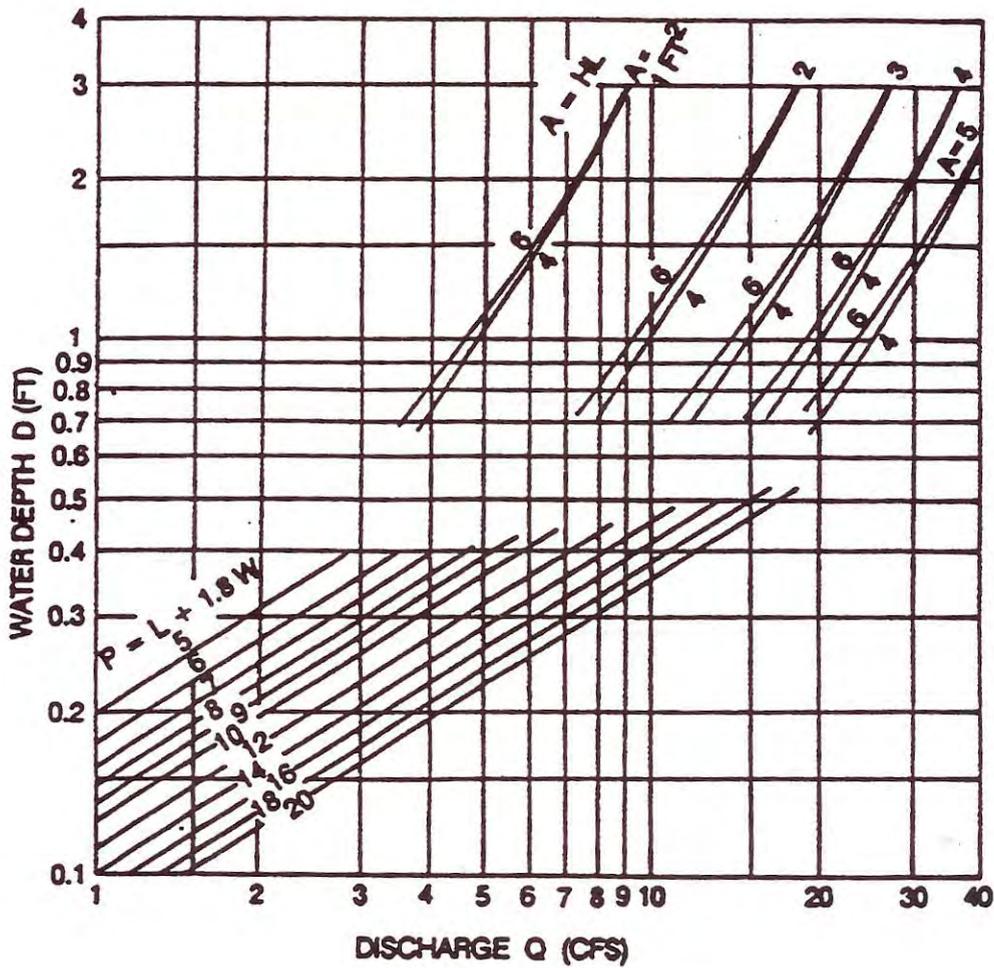
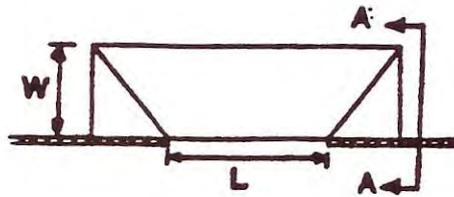
22

D. C. D. M. G.
 DIRECTOR 4/19/96
 DATE

CITY OF MANASSAS, VIRGINIA
 DEPARTMENT OF PUBLIC WORKS



SECTION A-A



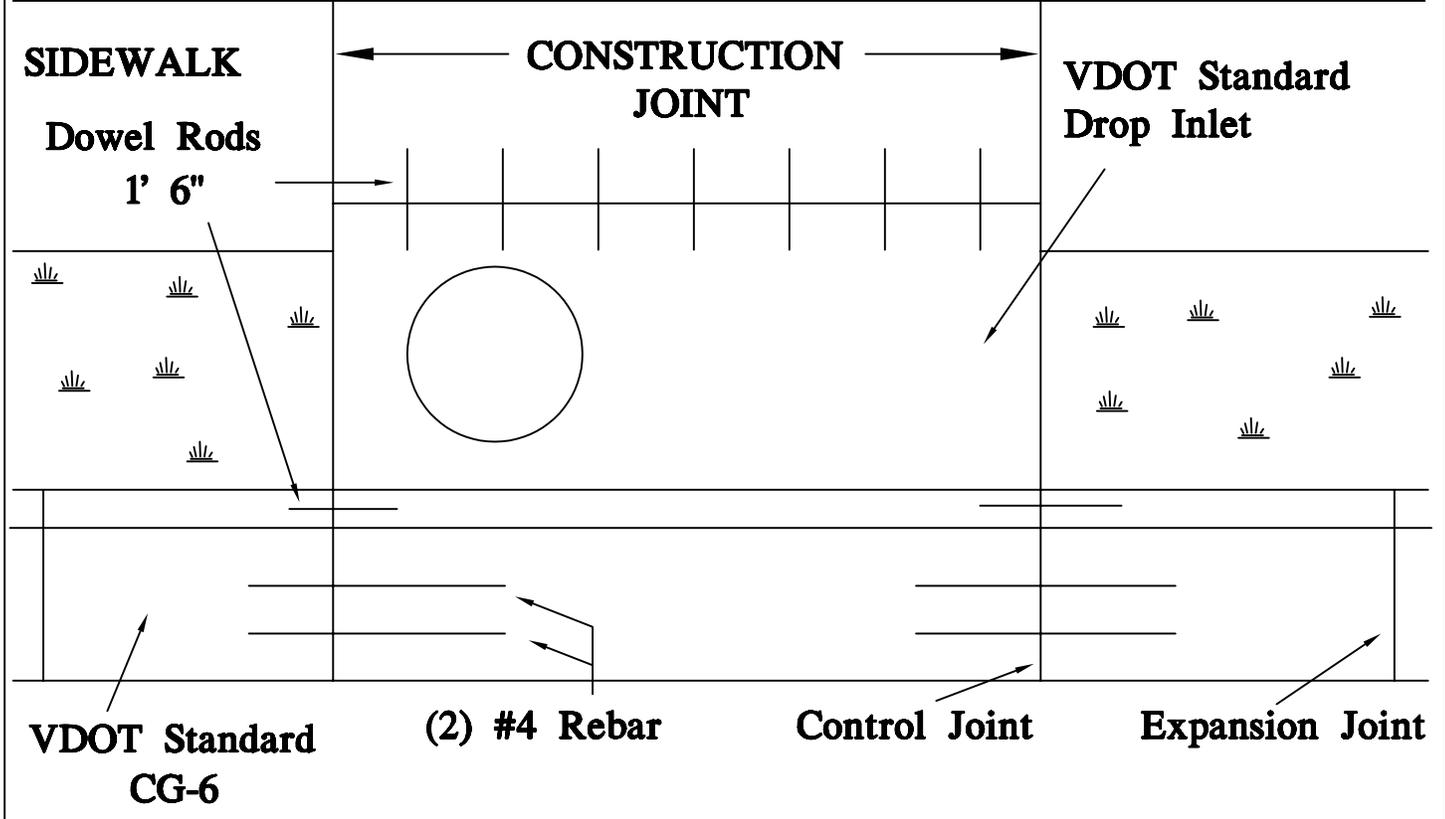
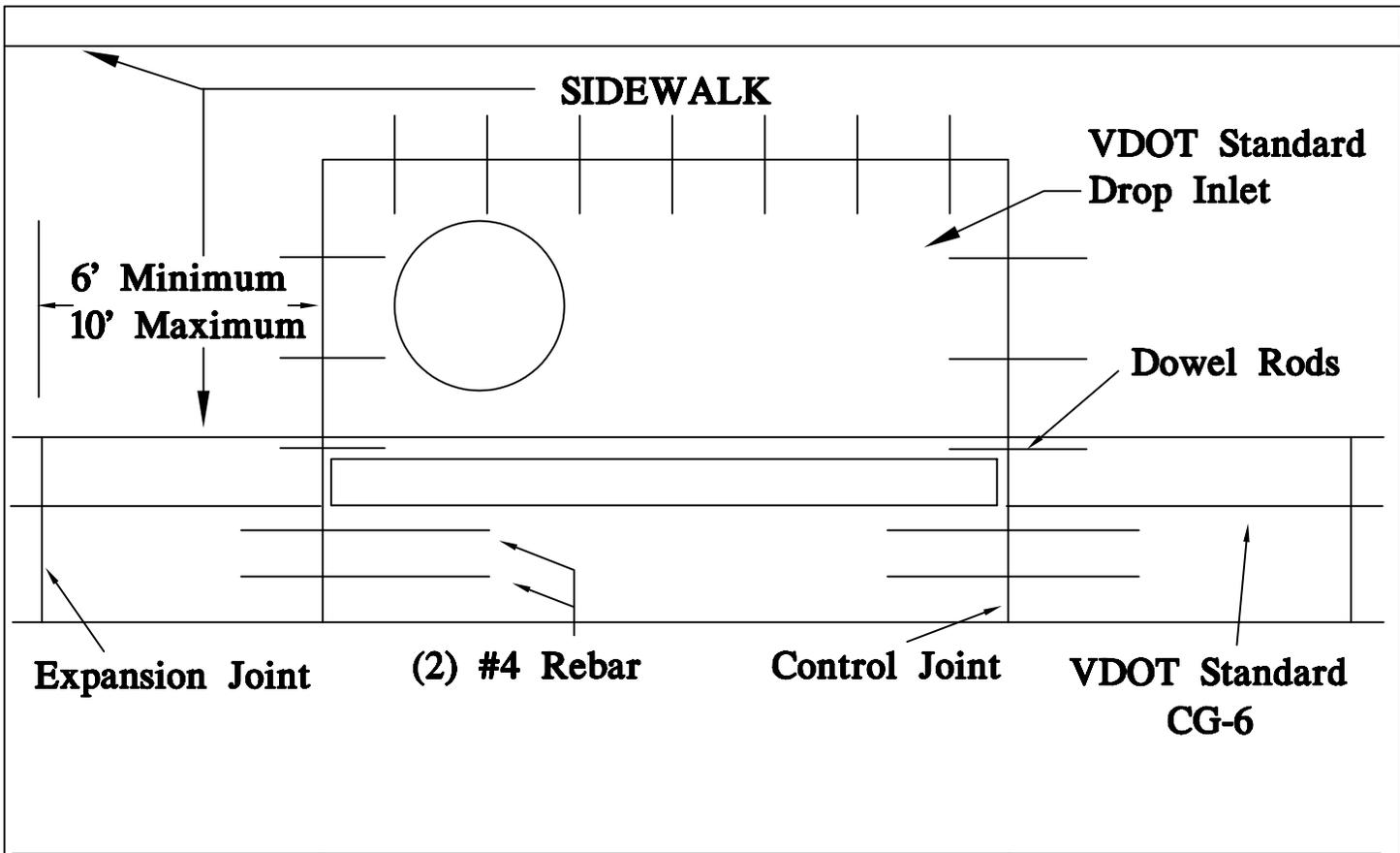
CURB INLET DESIGN CHART SUMP CONDITION

REVISION & DATE

EXHIBIT NUMBER

M.C. May 4/19/96
 DIRECTOR DATE

CITY OF MANASSAS, VIRGINIA
 DEPARTMENT OF PUBLIC WORKS



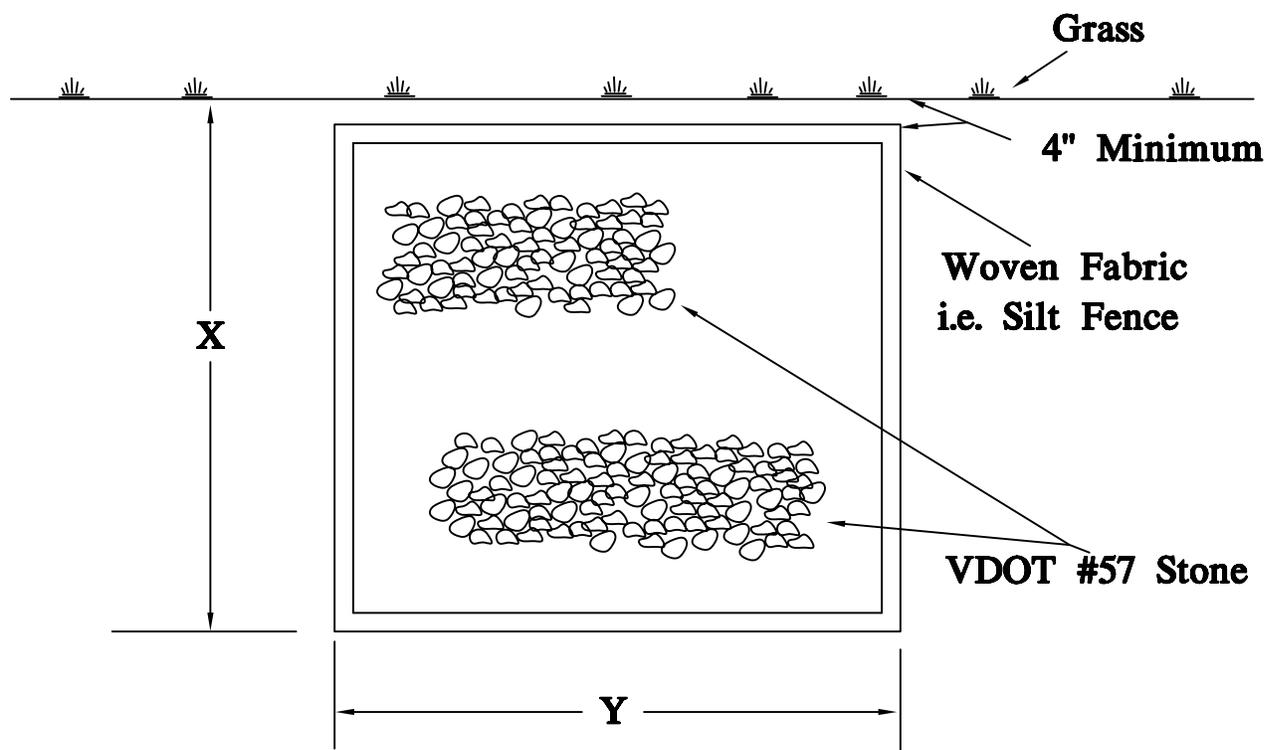
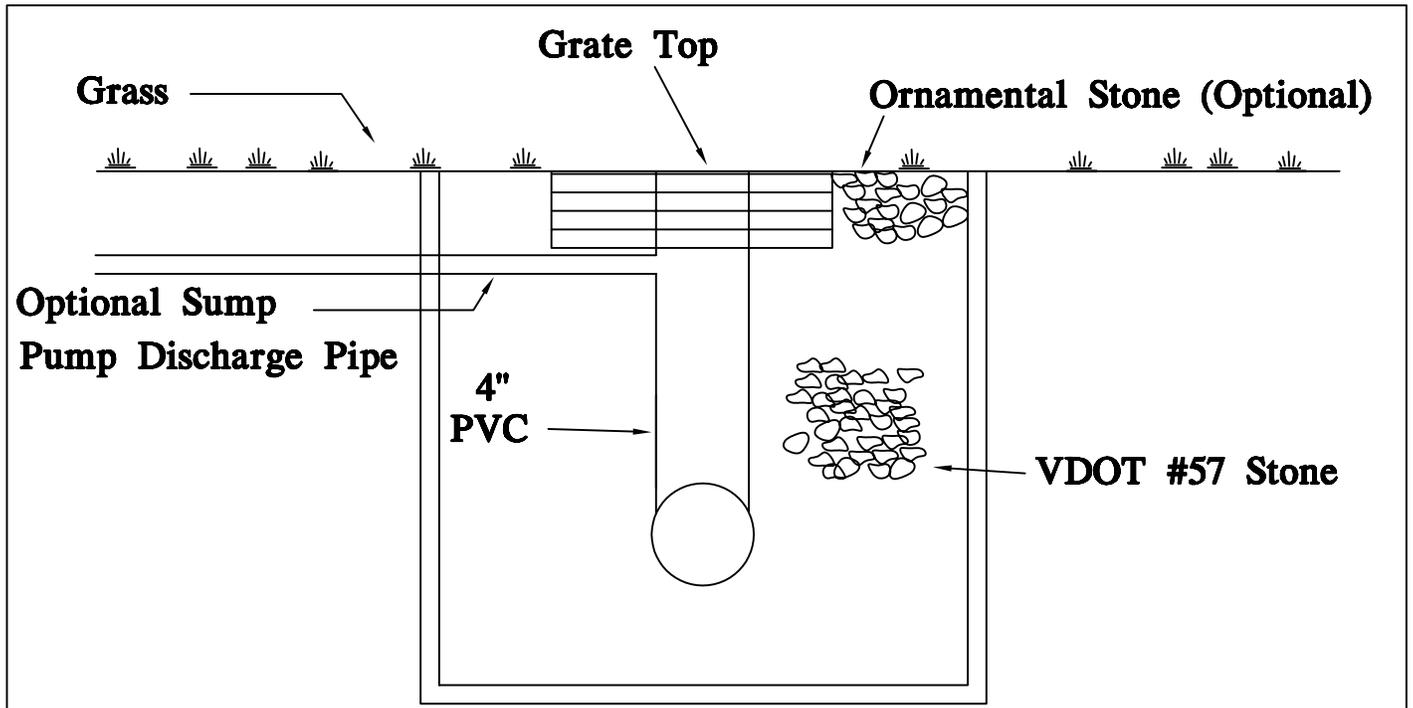
REINFORCEMENT DETAIL FOR DROP INLETS

REVISION & DATE	
EXHIBIT NUMBER	

[Signature] 5/1/04
DIRECTOR **DATE**

CITY OF MANASSAS, VIRGINIA
DEPARTMENT OF PUBLIC WORKS

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X = Approx. 4-6' deep of Fine Material

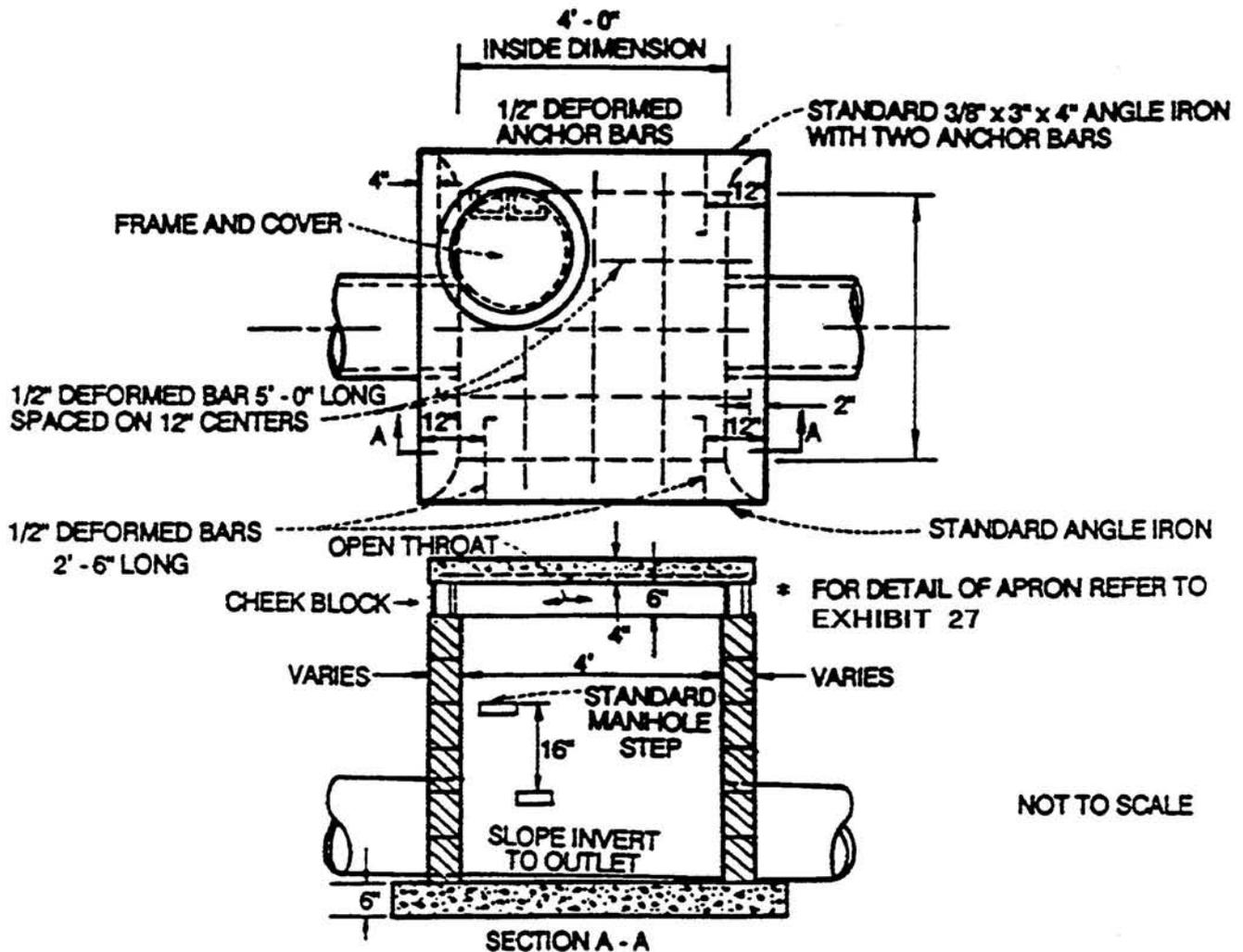
Y = Minimum of 6' x 6'

DRY WELL

REVISION & DATE	
EXHIBIT NUMBER	
25	

[Signature] 4/19/96
DIRECTOR **DATE**

**CITY OF MANASSAS, VIRGINIA
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- A. YARD INLETS DEEPER THAN 4 FEET SHALL HAVE STEPS AS SHOWN.
- B. DIMENSIONS OF YARD INLET SHOWN IS FOR PIPE SIZES UP TO AND INCLUDING 36 INCHES DIA. PIPE, WHILE PROVIDING A MINIMUM OF 6 INCHES OF CLEARANCE FROM THE INSIDE WALL OF THE STRUCTURE.
- C. INLETS FOR SIZES LARGER THAN 36 INCHES (DIA) WILL REQUIRE A SPECIAL DESIGN.
- D. SYMMETRICAL CHANNELS SHALL BE FORMED IN THE INVERT OF THE BOX FROM THE INLET PIPE TO THE OUTLET PIPE PER V.D.O.T. IS - 1 STANDARD.
- E. ANGLE IRON SHALL BE ASPHALT COATED.
- F. THE INSIDE AND OUTSIDE WALLS, AS THEY ARE LAID, SHALL BE PLASTERED WITH MORTAR A MINIMUM OF 1/2" THICK WHEN THE INLET IS CONSTRUCTED OF SOLID BLOCK.
- G. ALL YARD INLETS MUST HAVE APRONS AT ALL THROATS UNLESS APPROVED BY THE DIRECTOR.

* INLET CAGES ARE REQUIRED IN ALL RESIDENTIAL DEVELOPEMENTS

YARD INLET

REVISION & DATE

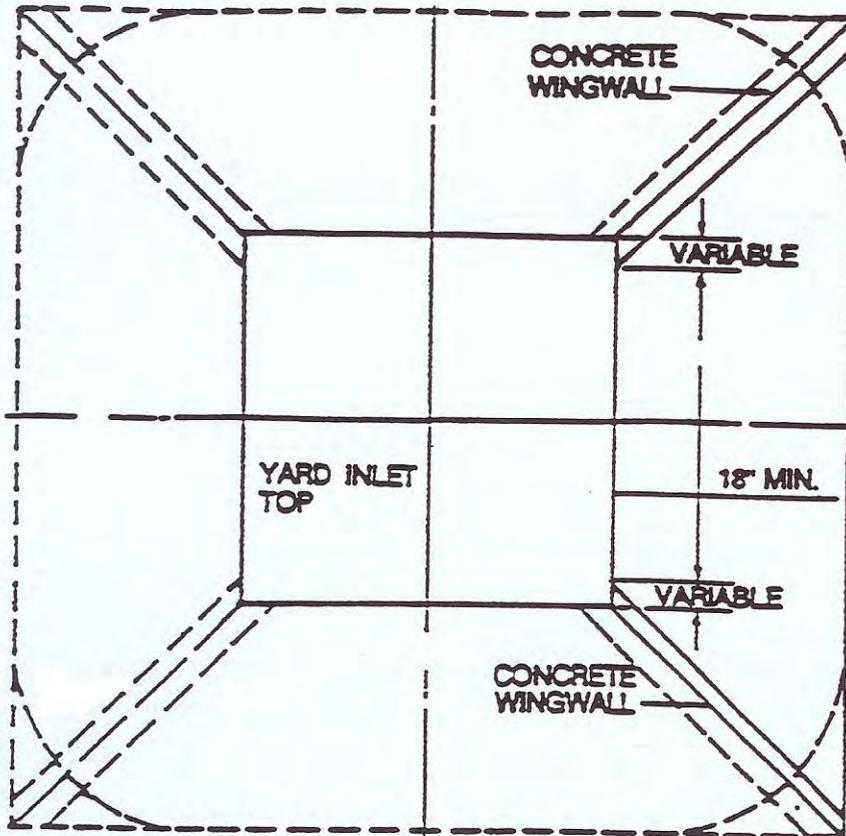
EXHIBIT NUMBER

DIRECTOR

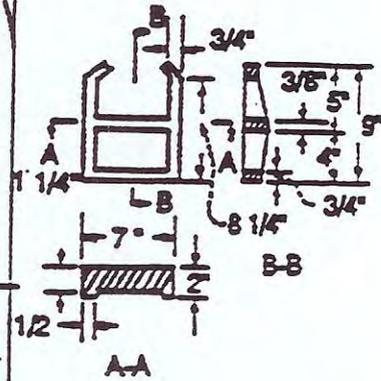
DATE

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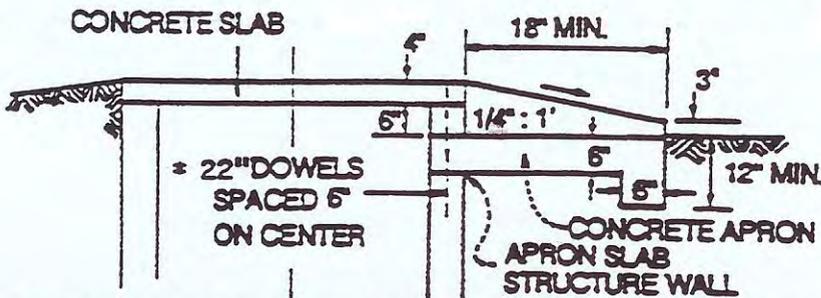
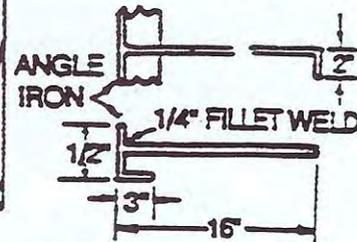
26



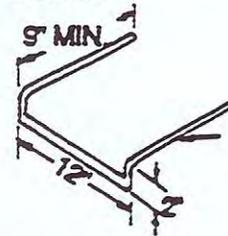
ALTERNATE STEP DETAIL



ANCHOR BAR DETAIL PLAN



STEP DETAIL



- A. WHEN APRONS ARE ON ADJACENT SIDES OF THE INLET, THE ADJOINING WINGWALLS SHALL BE OMITTED AND THE APRON SHALL HAVE A 1.5' RADIUS.
- B. WHEN THE INLET IS LARGER THAN 5' x 5' OPPOSITE CONCRETE APRONS SHALL BE CONSTRUCTED ON THE CENTERLINE OF THE INLET; TWO ADJACENT APRONS SHALL BE BUILT ADJOINING THE COMMON CORNER; IF THERE ARE THREE OR FOUR APRONS ON ONE INLET, THEN ALL SHALL BE BUILT ON CENTERLINE.
- C. NO. 6 GALVANIZED STEEL BAR OR NO. 3 REINFORCING ROD COMPLETELY ENCASED IN CORROSION RESISTANT RUBBER VINYL OR EPOXY.
- D. REINFORCING STEEL SHALL BE 6" x 6" NO. 6 WIRE MESH. NOT TO SCALE
- E. INLET CAGES ARE REQUIRED IN ALL RESIDENTIAL DEVELOPEMENTS

CONCRETE APRON FOR YARD INLETS

REVISION & DATE

EXHIBIT NUMBER

M.C. May 4/19/96
DIRECTOR DATE

CITY OF MANASSAS, VIRGINIA
DEPARTMENT OF PUBLIC WORKS

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STORMWATER MANAGEMENT FACT SHEET

 3/4/97
 _____ DATE
 DIRECTOR

**CITY OF MANASSAS, VIRGINIA
 DEPARTMENT OF PUBLIC WORKS**

REVISION & DATE

EXHIBIT NUMBER
28

SWM FACILITY INFORMATION

Basin Name _____
 Subbasin _____
 Stream Name _____
 Drainage Area (acres) _____
 draining to the facility _____
 Avg. Basin Slope (ft/ft) _____
 Type of facility _____
 (a) Dry pond _____
 (b) Wet pond _____
 (c) Park lot storg. _____
 (d) Rooftop storg. _____
 (e) Underground storg. _____
 (f) Porous pavement _____
 (g) Storm drains _____
 (h) Land cover control _____
 (i) Other _____
 Is the facility ON - SITE _____
 Is the facility OFF - SITE _____
 C.O.M. File # _____
 Development Name _____
 Tax Map # _____
 Was a fldpln. study prepared _yes _no
 If yes, File # _____
 Facility designed by: _____
 (Engr. Firm)

DESIGN INFORMATION (*)

Were hydrologic & hydraulic models developed _yes _no
 (a) Hydrologic Models (b) Hydraulic Models
 HEC-1 __ TR-20 __ HEC-1 __ WSP-20 __
 Other _____
 Method used to develop hydrographs _____
 Hydrograph routing methodology _____
 Reservoir routing methodology _____
 If the facility was not modeled, were elevation-discharge-storage
 tables developed _yes _no
 Outlet structure type _____
 Emergency spillway type _____
 Were elev.-disch. tables for the emer. spway. developed _yes _no
 Dam height (ft) ____, Invert elev. upst. ____, dwnst. ____
 Rainfall depth (inches) 2-yr. ____, 10-yr. ____, 100-yr. ____
 Rainfall depth (in.) 2-yr. ____, 10-yr. ____, 100-yr. ____
 Rainfall duration (hrs.) ____, Rainfall distribution _____
 Exist peak inflows (cfs) 2-yr. ____, 10-yr. ____, 100-yr. ____
 Devlp. peak inflows (cfs) 2-yr. ____, 10-yr. ____, 100-yr. ____
 Devlp. peak outflow (cfs) 2-yr. ____, 10-yr. ____, 100-yr. ____
 Water surface elev. (ft.) 2-yr. ____, 10-yr. ____, 100-yr. ____
 Reservoir storage (ac-ft.) 2-yr. ____, 10-yr. ____, 100-yr. ____
 Surface area (acres) 2-yr. ____, 10-yr. ____, 100-yr. ____
 Normal pool elevation (ft.) ____, Storage (ac-ft.) ____
 Surface area (acres) _____
 (*) For facilities type (a) and (b). For other types provide rainfall
 intensities data, storage vol., and discharges, if applicable.

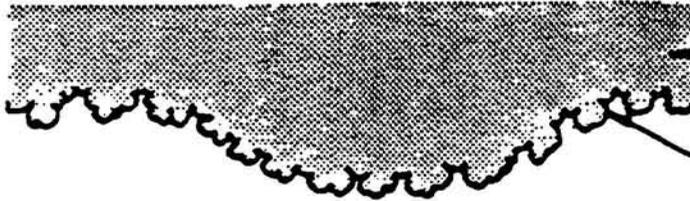
Date: _____

MISCELLANEOUS

Is additional storage capacity necessary to correct an existing problem __ yes __ no
 Does the facility incorporate BMP structural controls _ yes _ no
 If no, does the facility regulate the 2-yr. storm _ yes _no
 Was a description of the operation and maintenance needs of the facility included in the plans. _ yes _ no
 Back up data location plan ____, sheets ____, report ____, pages ____
 SWM bond estimate (\$) _____
 To be completed by C.O.M. staff
 Facility # _____
 Upstream POI _____
 Downstream POI _____
 Do the C.O.M. H & H models need to be updated _ yes _ no
 Model updated ___/___/___
 COM engineer _____
 Comments _____



THE APPARENT SIZE OF A POND IS INFLUENCED BY ITS SURROUNDING VEGETATION.



EXISTING TREES

IRREGULAR CLEARING EDGE



RECOMMENDED



EXISTING TREES

STRAIGHT CLEARING EDGE



NOT RECOMMENDED

EDGE TREATMENT OF PONDS

REVISION & DATE

EXHIBIT NUMBER

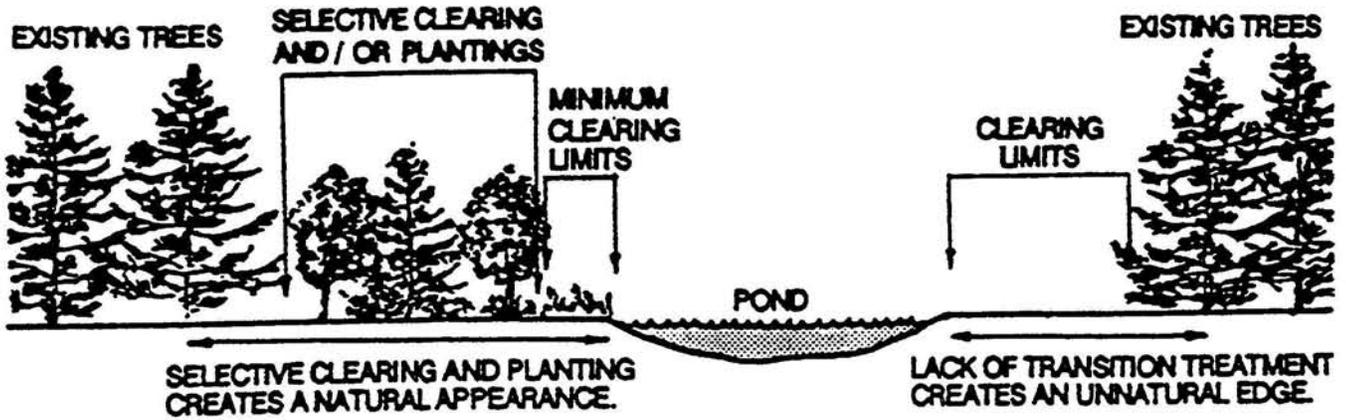
D. C. May
 DIRECTOR 4/19/96
 DATE

CITY OF MANASSAS, VIRGINIA
 DEPARTMENT OF PUBLIC WORKS

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RECOMMENDED

NOT RECOMMENDED



EXCAVATED AREA FINAL EDGE

WET POND EDGE TREATMENT

REVISION & DATE

EXHIBIT NUMBER

D. C. Drey 4/19/96
DIRECTOR DATE

CITY OF MANASSAS, VIRGINIA
DEPARTMENT OF PUBLIC WORKS

30



RECOMMENDED



NOT RECOMMENDED

EXCAVATED MATERIAL RESPREAD

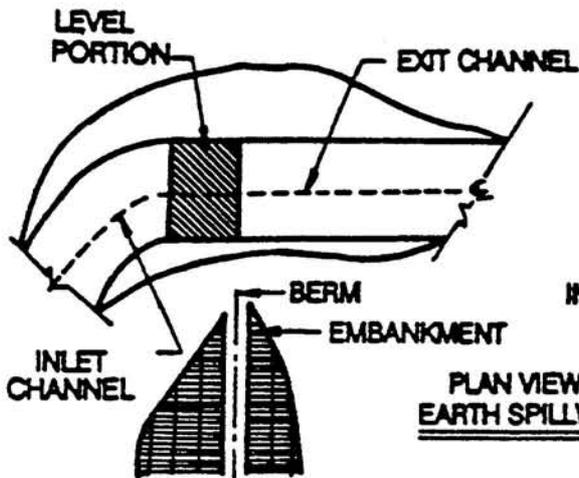
REVISION & DATE

EXHIBIT NUMBER

[Signature]
 DIRECTOR 4/19/96
 DATE

CITY OF MANASSAS, VIRGINIA
 DEPARTMENT OF PUBLIC WORKS

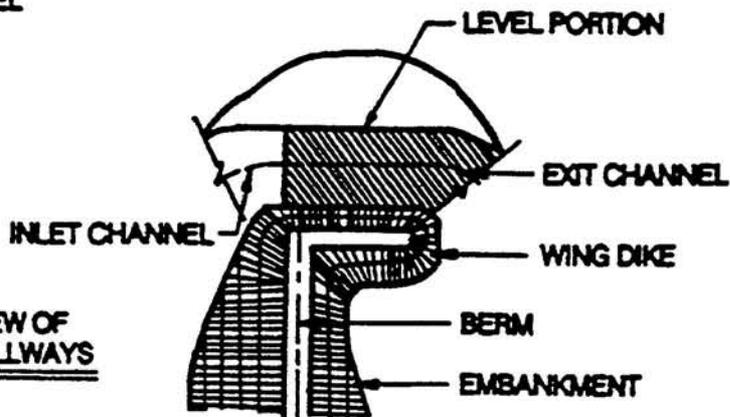
31



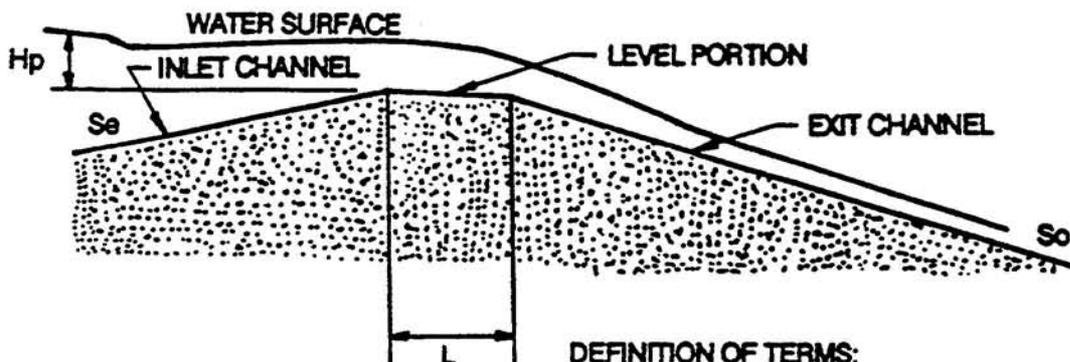
PLAN VIEW OF EARTH SPILLWAYS

EXCAVATED EARTH SPILLWAY

NEITHER THE LOCATION NOR THE ALIGNMENT OF THE LEVEL PORTION NEEDS TO COINCIDE WITH THE CENTERLINE OF THE DAM EMBANKMENT.



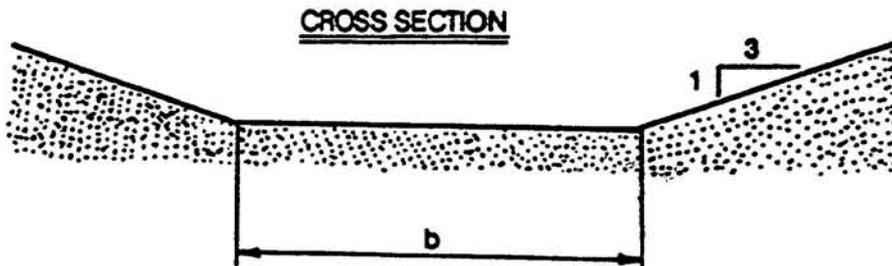
OPTIONAL WITH SOD OR RIPRAP ON WING SIDE
 CARE SHALL BE EXERCISED TO KEEP MACHINERY AND TRAFFIC OUT OF THE SPILLWAY DISCHARGE AREA TO PROTECT CHANNEL LINING.



PROFILE ALONG CENTERLINE

DEFINITION OF TERMS:

- Hp = DEPTH OF WATER IN POND ABOVE CREST
- L = LENGTH OF LEVEL PORTION (25' MINIMUM)
- b = BOTTOM WIDTH OF SPILLWAY
- So = SLOPE FOR EXIT CHANNEL
- Se = SLOPE OF INLET CHANNEL



NOT TO SCALE

EMBANKMENTS AND SPILLWAYS

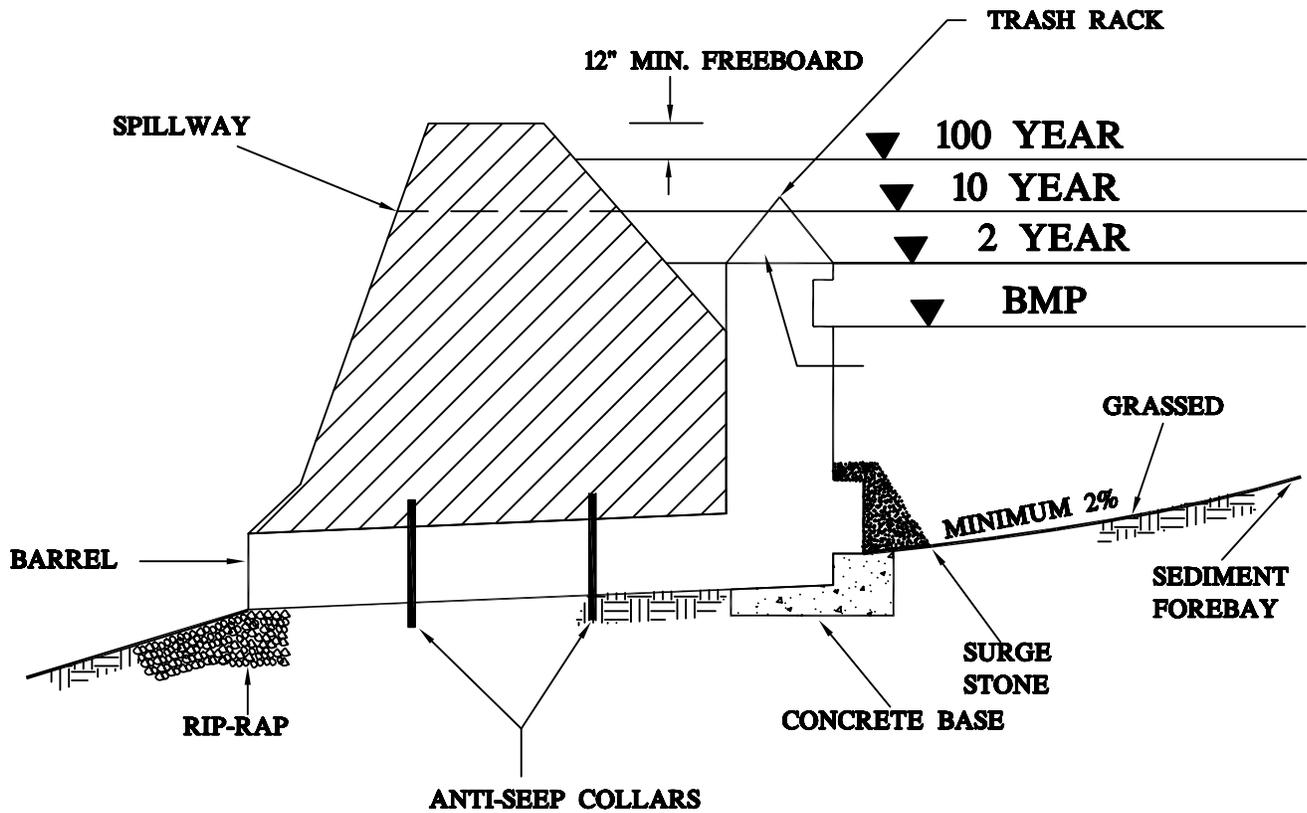
REVISION & DATE

EXHIBIT NUMBER

32

M.C. Dwyer 4/19/96
 DIRECTOR DATE

CITY OF MANASSAS, VIRGINIA
 DEPARTMENT OF PUBLIC WORKS



NOT TO SCALE

**TYPICAL DRY
POND**

REVISION & DATE

EXHIBIT NUMBER

33

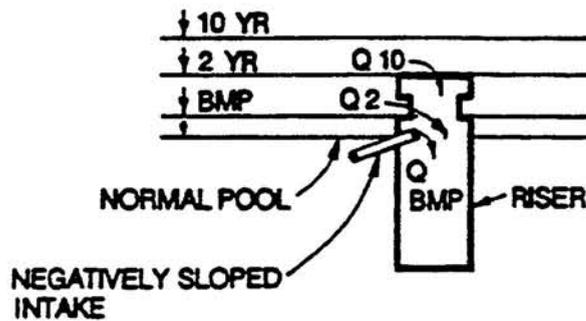
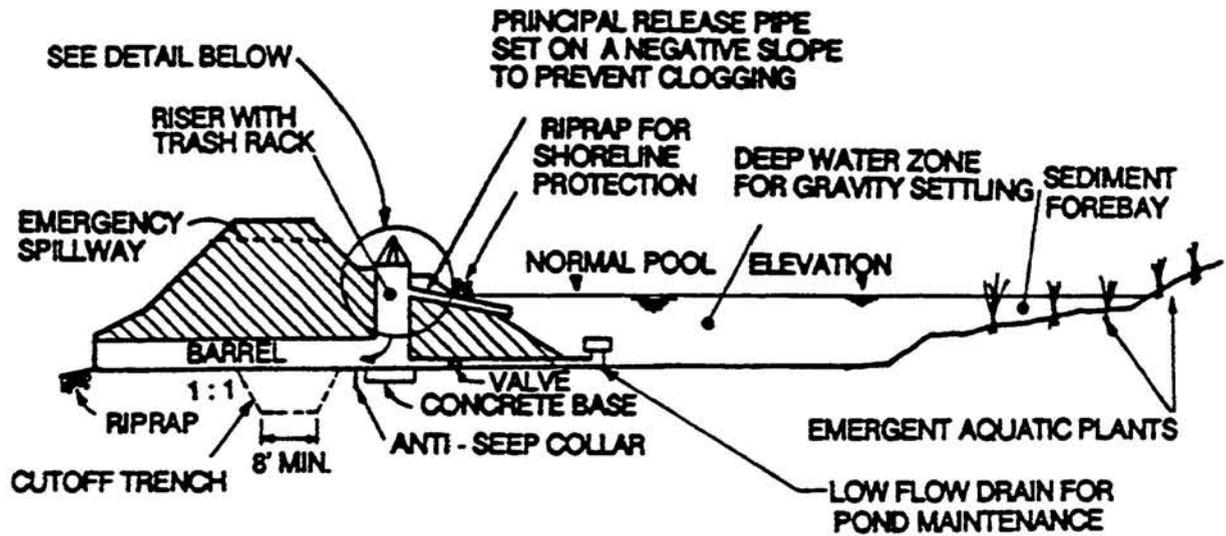
[Signature]

4/19/96

DIRECTOR

DATE

**CITY OF MANASSAS, VIRGINIA
DEPARTMENT OF PUBLIC WORKS**



NOT TO SCALE

TYPICAL WET POND

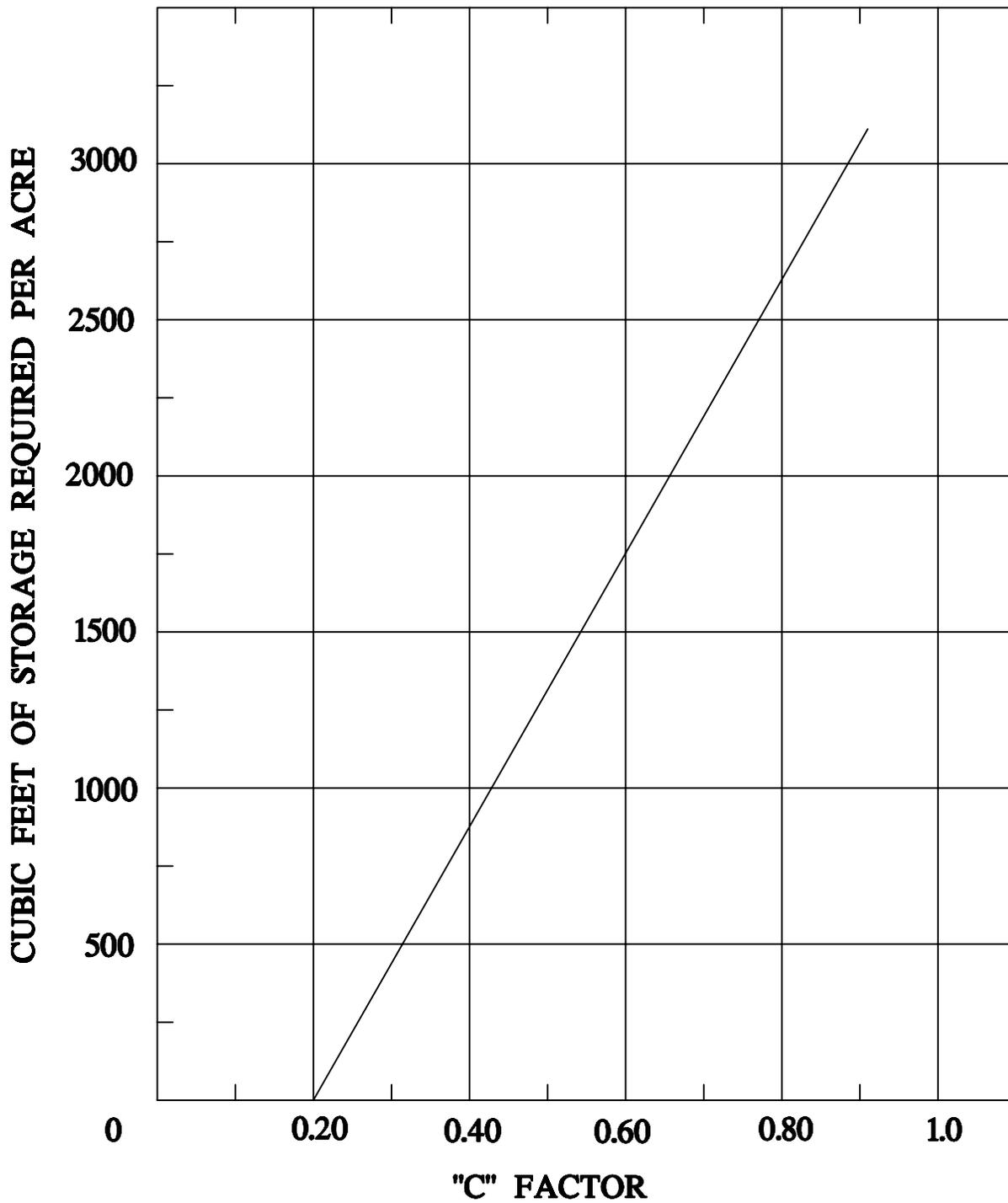
REVISION & DATE

EXHIBIT NUMBER

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[Signature]
DIRECTOR
4/19/96
DATE



WATER QUALITY REQUIREMENTS

REVISION & DATE	

EXHIBIT NUMBER	

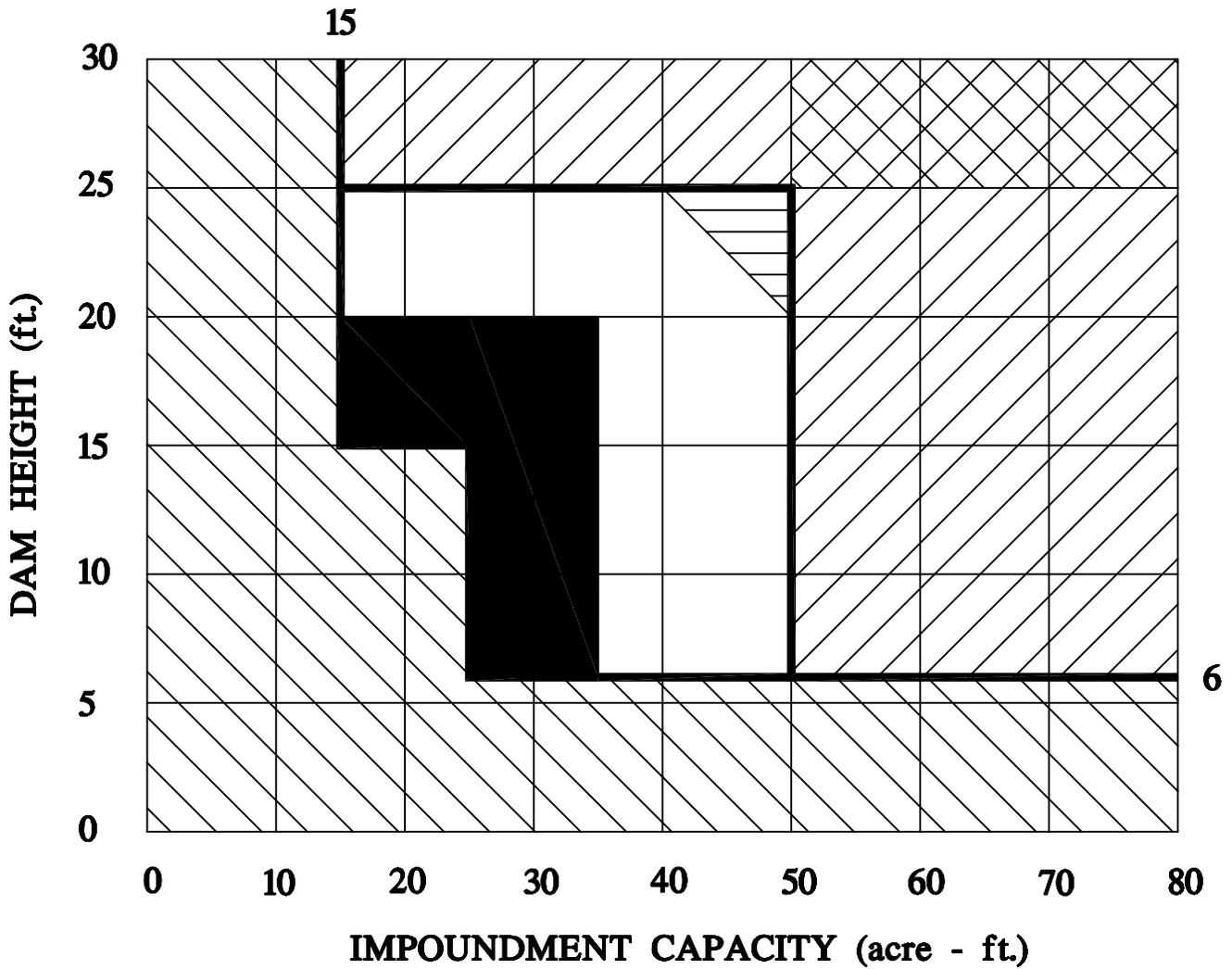
Paul C. Miller 5/3/96

DIRECTOR

DATE

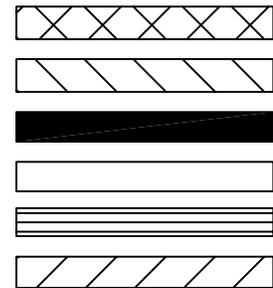
**CITY OF MANASSAS, VIRGINIA
DEPARTMENT OF PUBLIC WORKS**

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DAMS REGULATED BY THE DEPARTMENT OF CONSERVATION AND HISTORIC RESOURCES

- 1 (100 yr.) = PMF DESIGN MINIMUM
- 1.5 (100 yr.) = 0.3 PMF
- 2.0 (100 yr.) = 0.4 PMF
- 2.5 (100 yr.) = 0.5 PMF
- 5.0 (100 yr.) = 1.0 PMF



PMF = probable maximum flood

DESIGN STORM FOR DAMS

REVISION & DATE

EXHIBIT NUMBER

Paul C. Miller

4/19/96

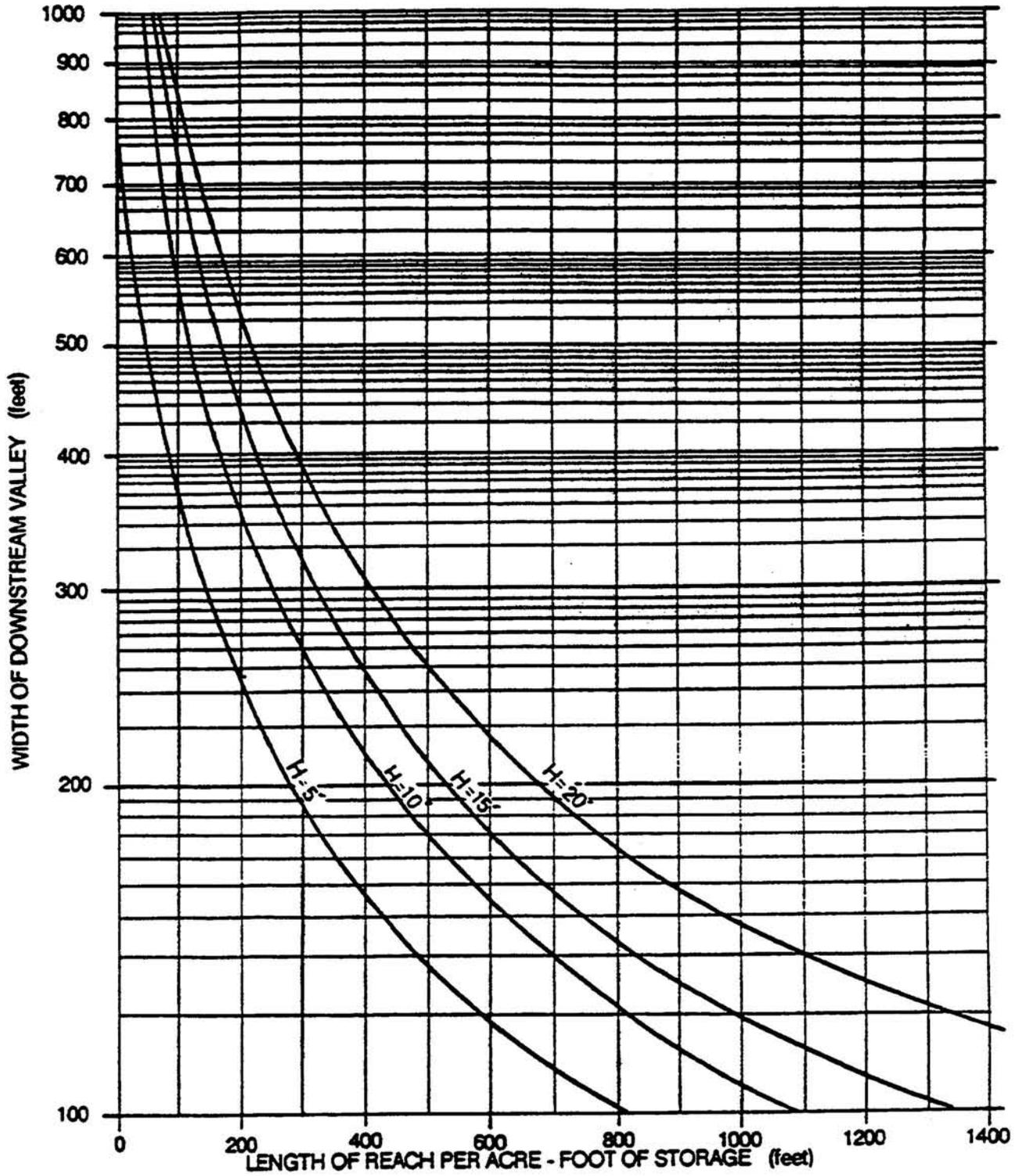
DIRECTOR

DATE

CITY OF MANASSAS, VIRGINIA
DEPARTMENT OF PUBLIC WORKS

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H EQUAL TO DAM HEIGHT



DANGER REACH LENGTH

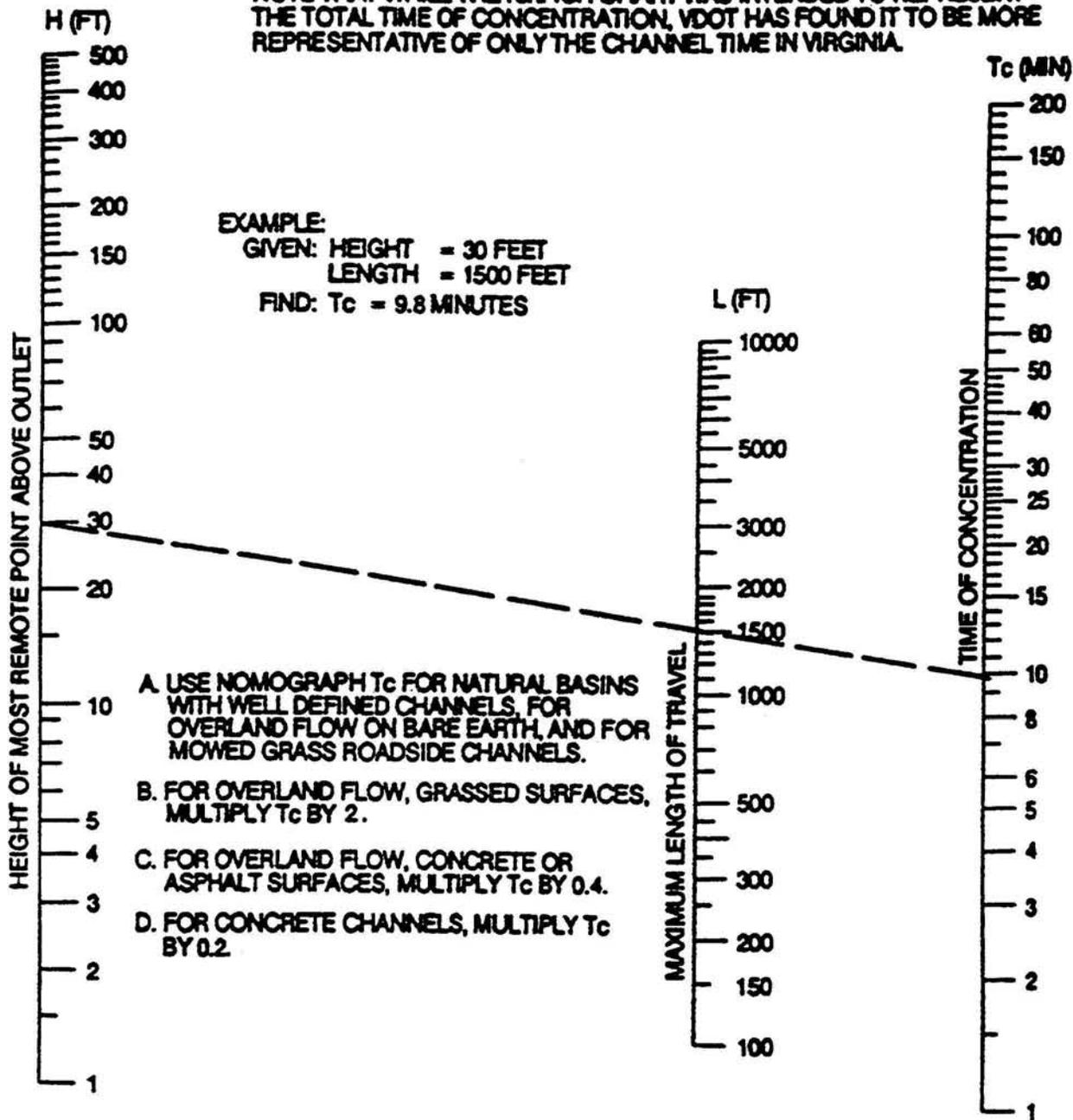
D. C. Drey
DIRECTOR

4/19/60
DATE

CITY OF MANASSAS, VIRGINIA
DEPARTMENT OF PUBLIC WORKS

REVISION & DATE
EXHIBIT NUMBER
37

NOTE THAT WHILE THE KIRPICH CHART WAS INTENDED TO REPRESENT THE TOTAL TIME OF CONCENTRATION, VDOT HAS FOUND IT TO BE MORE REPRESENTATIVE OF ONLY THE CHANNEL TIME IN VIRGINIA.



BASED ON STUDY BY P.Z. KIRPICH

TIME OF CONCENTRATION SMALL BASINS

REVISION & DATE

EXHIBIT NUMBER

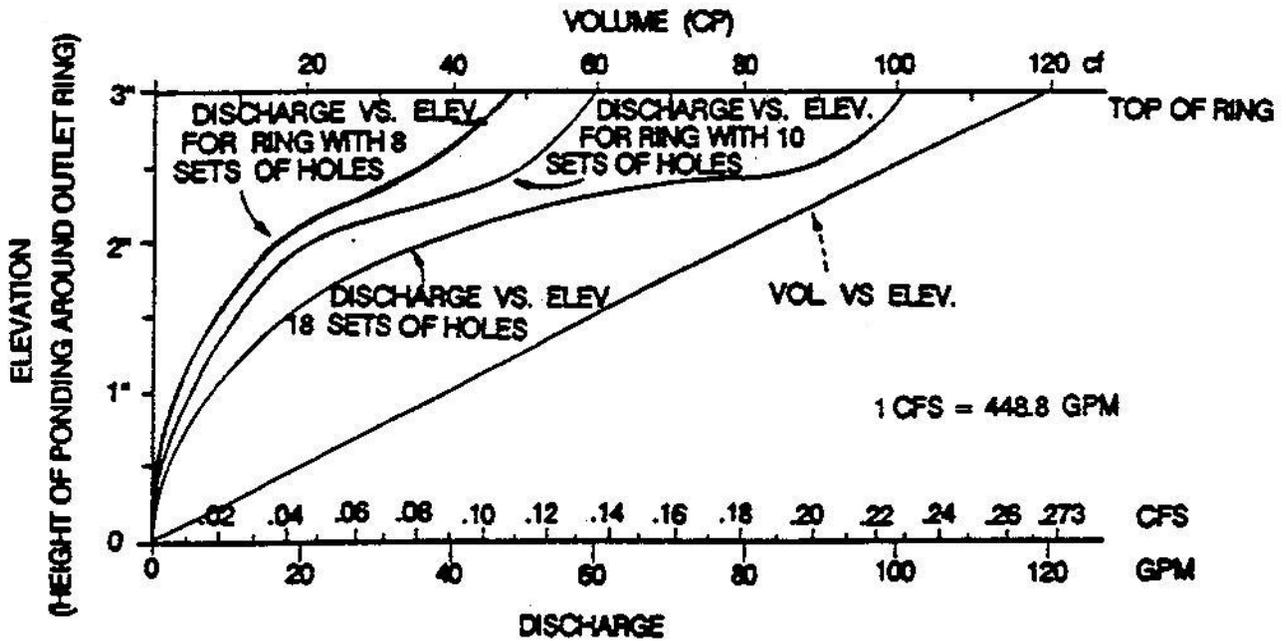
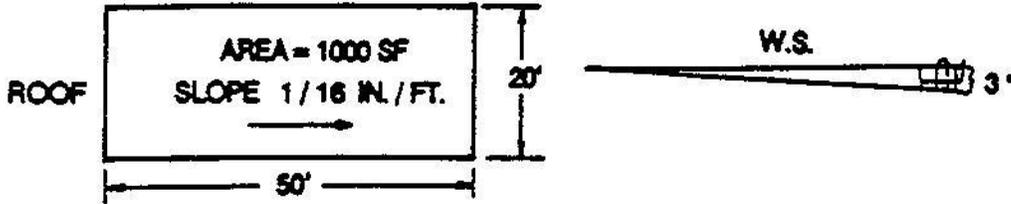
P. C. May 4/19/96
 DIRECTOR DATE

CITY OF MANASSAS, VIRGINIA
 DEPARTMENT OF PUBLIC WORKS

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CAPACITY THROUGH HOLES				
WATER DEPTH AT INLET (INCHES)	DISCHARGE (GPM)			
	1 SET HOLES	8 SETS	10 SETS	18 SETS
1.5	1	8	10	18
2.0	2	16	20	36
2.5	3	40	50	90
3.0	6	48	60	108

ROOFTOP DETENTION PERFORMANCE CURVE



ROOF TOP STORM WATER DETENTION

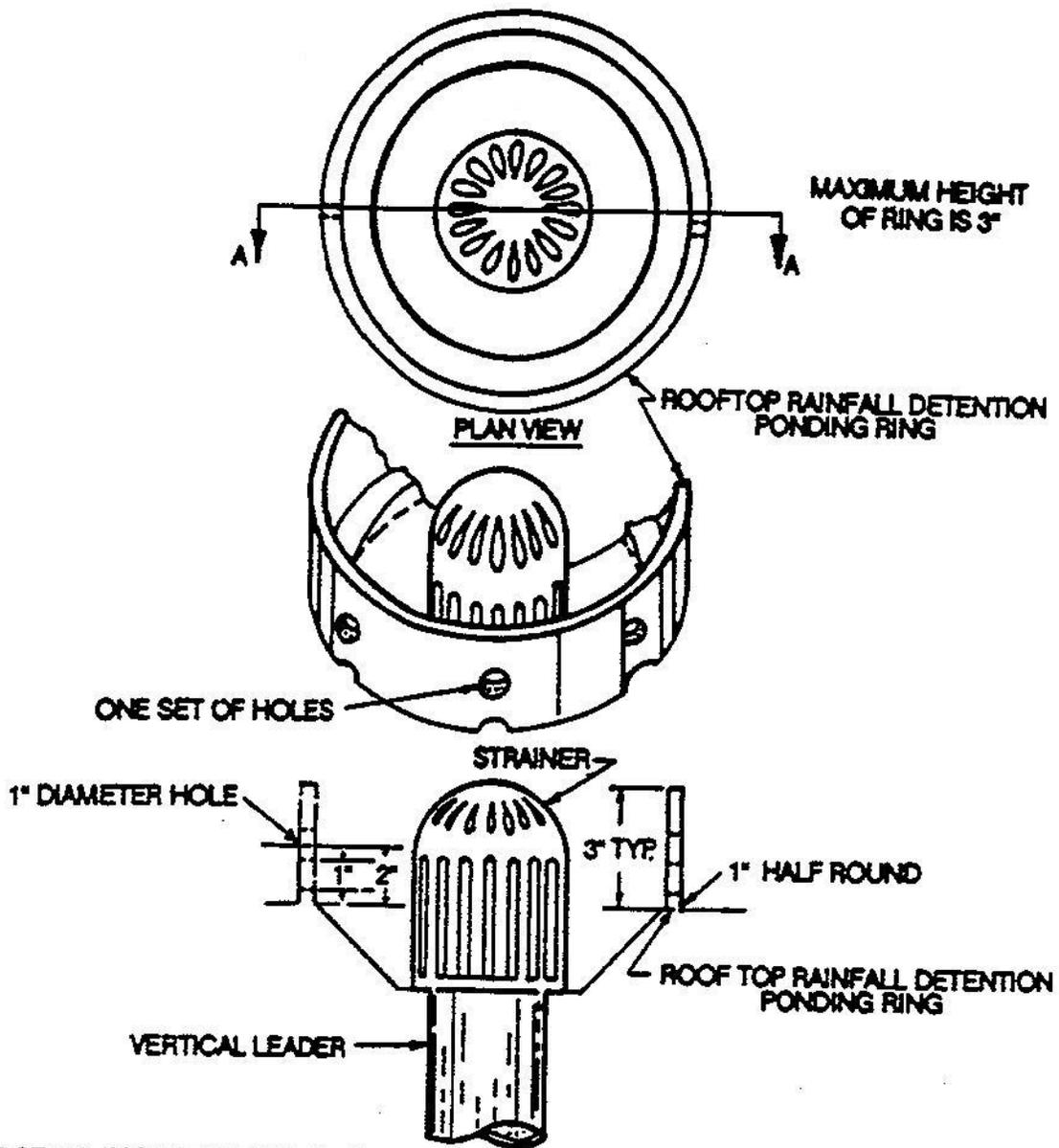
M. C. D. May 4/19/96
DIRECTOR DATE

CITY OF MANASSAS, VIRGINIA
DEPARTMENT OF PUBLIC WORKS

REVISION & DATE

EXHIBIT NUMBER

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A. BRASS OR STAINLESS STEEL RING PLACED AROUND STANDARD ROOF DRAIN.

B. RING HEIGHT AND DIAMETER AND NUMBER AND SIZES OF HOLES ARE DETERMINED BY THE ROOF AREA DRAINED, THE NUMBER OF DRAINS, AND THE RAINFALL DESIGN CRITERIA.

NOT TO SCALE

ROOFTOP RAINFALL PONDING RING

REVISION & DATE

EXHIBIT NUMBER

40

CITY OF MANASSAS, VIRGINIA
DEPARTMENT OF PUBLIC WORKS

DIRECTOR

DATE

4/19/96

REQUEST FOR STORMWATER WAIVER FORM

Name of Owner: _____

Address: _____

Phone: _____

Engineer: _____

RE (Site Name): _____

Waiver Category: _____

I hereby request that the City of Manassas waive the requirement for stormwater management for the above-named site. I believe that my development falls into the waiver category indicated above based on the following information which I hereby certify as being accurate.

Proposed amount of disturbed area: _____ **Acres**

Proposed amount of impervious area: _____ **Acres**

I understand that if any changes are made in the above figures, I will notify the City of Manassas in writing.

I further understand that I will receive written notification from the City of Manassas informing me of the status of this request within 30 days of receipt by the Department of Public Works.

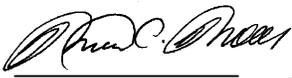
Date:

Owner's Signature

Attachment: Site development plan showing existing and proposed grading, including information concerning the outfall and receiving downstream conditions.

STORMWATER WAIVER FORM

REVISION & DATE	
EXHIBIT NUMBER	
44	

 4/19/96

DIRECTOR **DATE**

**CITY OF MANASSAS, VIRGINIA
 DEPARTMENT OF PUBLIC WORKS**

REQUEST FOR ON-SITE DETENTION WAIVER FORM

Four (4) copies of the following information should be submitted to the City of Manassas Department of Public Works.

Subdivision (Record Plat Title) _____

Name of Owner: _____

Address: _____

Phone: _____

Engineer: _____

Address: _____

Phone: _____

Size of Tract _____ (Gross Ac.) No. of Lots _____ Zone _____

Watershed _____

Plat No. _____ Date _____

I hereby request that the City of Manassas waive the requirement for on-site detention for the above-named site. I understand that I will receive written notification from the City of Manassas informing me of the status of this request within 30 days of receipt by the Department of Public Works.

Date:

Owner's Signature

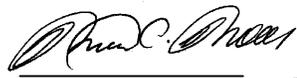
I believe that this request is justified based upon the attached information which I hereby certify as being accurate.

Date:

Professional Engineer's Signature

ON-SITE DETENTION WAIVER FORM

REVISION & DATE	
EXHIBIT NUMBER	
45	

 4/19/96

DIRECTOR DATE

**CITY OF MANASSAS, VIRGINIA
DEPARTMENT OF PUBLIC WORKS**

REQUEST FOR ON-SITE DETENTION WAIVER FORM

The following supporting information is to be provided as part of the request for waiver for on-site detention under Section 8-510.6:

1. **Location Map** - The map should outline development and watershed tributary to the proposed development.
2. **Proposed Plat** - (as available)
3. **Plan of Proposed Development** - The plan is to show streets, parking lots, topography, 100-year flood plains, easements for storm drains, sewers, and other utilities; major building locations (except single-family detached buildings); etc.
4. **Peak Flows For the 10-year, 6-hour storm** - Before and after development (without any on-site detention).
5. **Justification For Requesting Waiver** - In addition, the following would be useful in supporting the waiver request:
 - * Location of site and type of existing or proposed off-site central stormwater management structure and estimated available storage or alternate control measures.
 - * Peak flows for 10-year, 6-hour and 100-year, 24-hour storms computed before and after development and volume of storage to be provided for control of these storms.
 - * If applicable, availability of land rights for a proposed central stormwater management structure and preliminary cost estimate for land and construction.
6. **Related Drainage Area Studies** which may support the request for the waiver.

ON-SITE DETENTION WAIVER FORM

REVISION & DATE

EXHIBIT NUMBER

45 (cont.)



DIRECTOR

4/19/96

DATE

**CITY OF MANASSAS, VIRGINIA
DEPARTMENT OF PUBLIC WORKS**

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